

Preliminary Engineering Report

Water System Improvements

Scatchet Head Water District
PWS ID: 76470 X
Clinton, WA 98236

October 2020

For Submittal to:
Darla O'Connor
Community Programs
USDA Rural Development 2021 E.
College Way
Suite 216
Mount Vernon, WA 98273

System Owner:

Scatchet Head Water District
7906 Guemes Avenue
Clinton, WA 98236

Contact: David Mullins
Phone: (360) 578-7044



Davido Consulting Group

Seattle | Mount Vernon | Whidbey Island | Federal Way

P.O. Box 1132
Freeland, WA 98249
Tel 360.331.4131

**CERTIFICATE OF ENGINEER
Scatchet Head Water District
Water System Improvements**

The technical material and data contained within this report has been prepared by or under the direction of the following registered professional engineer(s), licensed in accordance with the laws of the State of Washington to practice in the State of Washington.



QUICK REFERENCE PROJECT INFORMATION

General Project Information

| | |
|--|---|
| Water System | Scatchet Head Water District |
| Water System ID | 76470 X |
| Project Description | Replace aging watermains, source pumps, and other treatment and source improvements |
| Reservoir, Pumphouse, and Well Parcel # | S8110-00-05013-0. |
| Consulting Engineer | Robert Bennion, PE – Davido Consulting Group, Inc. |

Project Summary

| Component | Description |
|----------------------------|--|
| Source | <p><u>S01- Well #1</u>: Abandoned</p> <p><u>S02- Well #2</u>: 1980 – 10” casing – 295’ deep Screened Interval: 231-234’ Static Water Level – 190’</p> <p><u>S03- Well #3</u>: 1995 – 8” casing – 403’ deep Screened Interval: 242-246’ Static Water Level – not recorded</p> |
| Submersible Pumps | <p><u>S02- Well #2</u> - 125 gpm, 30 HP pump, Goulds Model 160CLC030, 12 stage, 3450 rpm, 480/277 VAC, three phase</p> <p><u>S03- Well #3</u> - 66 gpm, Goulds Model 70J15, 15 HP, 13 stages, 3450 rpm, 480/277 VAC, three phase</p> |
| Reservoirs | <p>#1 – 300,000 gallon Guemes Avenue Reservoir: 24.0’ diameter x 85’ tall</p> <p>#2 – 120,000 gallon Maple Point Drive Reservoir: 14.6’ diameter x 95.0’ tall</p> |
| Booster Pump Station | <p>(4) Aurora Series 340 / 360, 7.5 HP, 3500 RPM – 200 gpm at 45 psi (260 gpm at 30 psi) Horizontal Pneumatic Tank - 2,120 gallon Canal Boiler Works 66” diameter x 10’ horizontal</p> |
| Structures | 1,125 SF Pumphouse |
| Chemical Injection Systems | Hypochlorinator – Pre and Post Treatment LMI Series A17 Pump: 2.0 GPH, 50 psi |
| Filtration | Iron and Manganese Reduction System (4) 48” Diameter, 463 Gallon Filter Tanks |
| Distribution System | <p>2” & 2.5” (various materials) – 6,636’</p> <p>4” (polyvinyl chloride, PVC) – 8,695’</p> <p>6” (asbestos cement, AC) – 9,755’</p> <p>6” (ductile iron, DI) – 940’</p> <p>6” (PVC, class 150) – 1,313’</p> <p>6” (C-900 PVC, class 150) – 11,034’</p> <p>8” (ductile iron, DI) – 312’</p> <p>8” (C-900 PVC, class 150) – 567’</p> |

TABLE OF CONTENTS

| | |
|--|-------------------------------------|
| 1. Project Planning..... | 1 |
| 1.1 Location | 1 |
| 1.2 Environmental Resources Present..... | 2 |
| 1.3 Population Trends..... | 3 |
| 1.4 Community Engagement | 4 |
| 2. Existing Facilities..... | 4 |
| 2.1 History..... | 4 |
| 2.2 Existing Conditions..... | 5 |
| 2.2.1 Source:..... | 5 |
| 2.2.2 Storage: | 6 |
| 2.2.3 Booster Pumps, Pressure tanks, and Controls: | 6 |
| 2.2.4 Distribution System:..... | 6 |
| 2.2.5 Treatment/Pumphouse:..... | 7 |
| 2.3 Financial Status of Any Existing Facilities | 8 |
| 2.4 Water/Energy/Waste Audits | 8 |
| 3. Need For Project | 9 |
| 3.1 Health, Sanitation and Security | 9 |
| 3.2 Aging Infrastructure..... | 9 |
| 3.3 Fire Flow | 9 |
| 3.4 Reasonable Growth | 9 |
| 4. Alternatives Considered | 10 |
| 4.1 No Action | 10 |
| 4.2 Distribution System Improvement Alternatives..... | 10 |
| 4.3 Pumphouse and Treatment Improvement Alternatives | Error! Bookmark not defined. |
| 4.4 Source Improvement Alternatives..... | 15 |
| 5. Selection of an Alternative | 15 |
| 5.1 Life Cycle Cost Analysis | 16 |
| 6. Proposed Project | 17 |
| 6.1 Preliminary Project Design | 17 |
| 6.2 Project Schedule | 18 |
| 6.3 Permit Needs | 18 |
| 6.4 Annual Operating Budget | 18 |
| 7. Conclusions and Recommendations..... | 19 |

APPENDICES

| | |
|------------|-------------------------------|
| APPENDIX A | Maps and Schematics |
| APPENDIX B | Water Facility Inventory Form |
| APPENDIX C | Asset Inventory |
| APPENDIX D | Financial Information |
| APPENDIX E | Water Use Efficiency Reports |
| APPENDIX F | Water Quality Results |
| APPENDIX G | Hydraulic Model |

LIST OF FIGURES

Figure 1: Locator map 1
Figure 2: Scatchet Head Water District Service Area..... 2
Figure 3: Sensitive Areas Map..... 3
Figure 4: Pressure Zone and Facilities Map 5

LIST OF TABLES

Table 1: SHWD Expenditures and Income for 2016, 2017, 2018 and 2020..... 8
Table 2: Distribution Improvement **Error! Bookmark not defined.**
Table 3: Improvement Alternatives Cost Estimate Summary..... **Error! Bookmark not defined.**
Table 4: Present Worth **Error! Bookmark not defined.**
Table 5: Interim Increasing Block Rate Structure 19

1. PROJECT PLANNING

The Scatchet Head Water District (SHWD) is a Group A Community water system currently providing potable water to 410 connections within its service area south of Clinton, WA. The SHWD is in the southern end of Whidbey Island in Island County, Washington. See Appendix A for a detailed service area map. Figure 1 below shows the approximate site location for this project. A summary of the system connections, sources, and contacts are included in the Water Facility Inventory (WFI) from provided in APPENDIX B.

The proposed project will replace aging water mains, provide fire flow capacity throughout the distribution system, and will include other improvements to the distribution system, treatment system and sources. The total proposed projects are expected to cost \$3,070,000.

1.1 Location

The water system is located on the southern end of Whidbey Island between Cultus Bay and Useless Bay as seen in Figure 1. The service area for the system is shown in Figure 2.

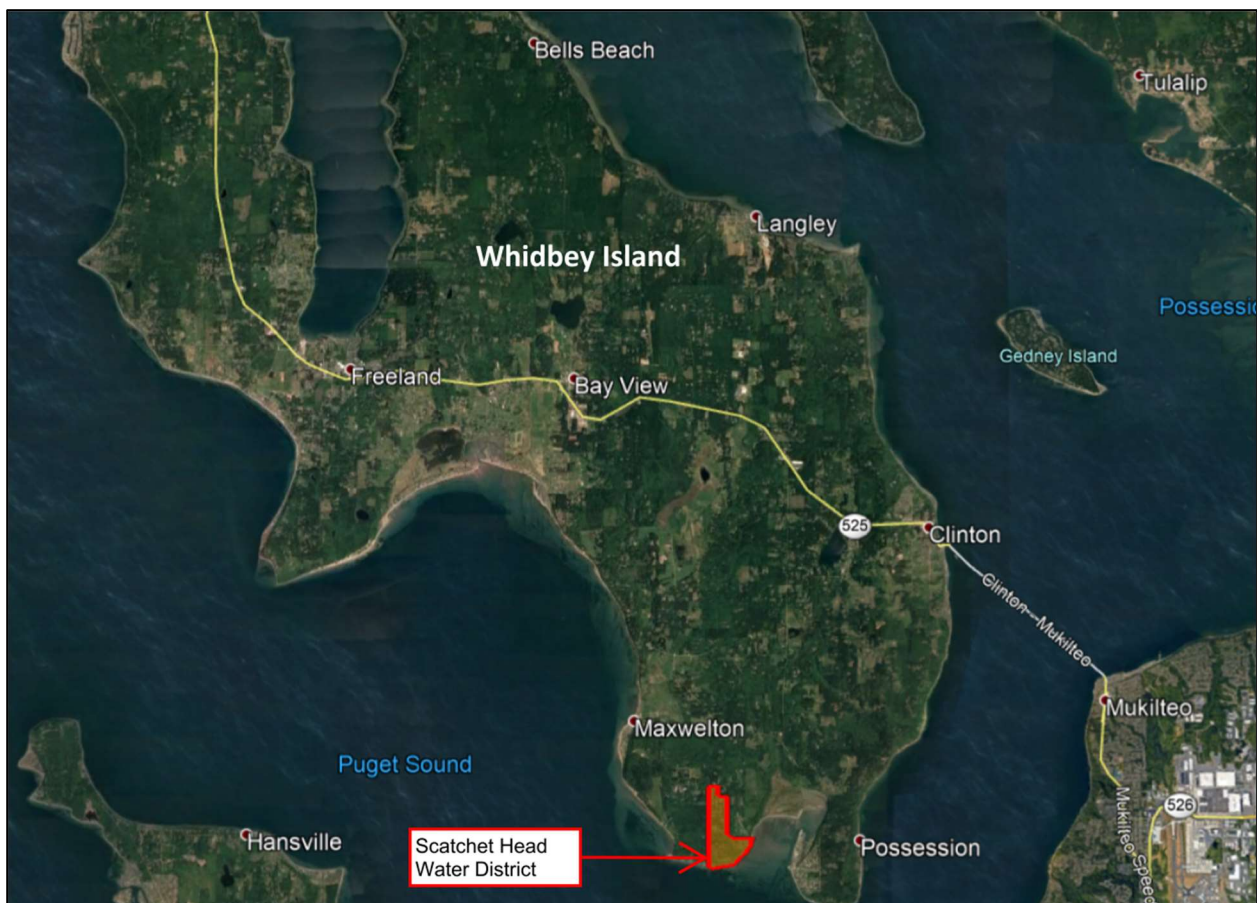


Figure 1: Locator map



Figure 2: Scatchet Head Water District Service Area

1.2 Environmental Resources Present

There are several sensitive areas within the SHWD as shown in Figure 3. Unstable slope areas are present at southern end of the service area along the coastline. Some streams and wetlands are also present within the service area. An environmental report is being developed to support this project. The environmental report will comply with the National Environmental Protection Act (NEPA) to support the loan application. The project is considered categorically exempt because it is replacing existing utility pipes.

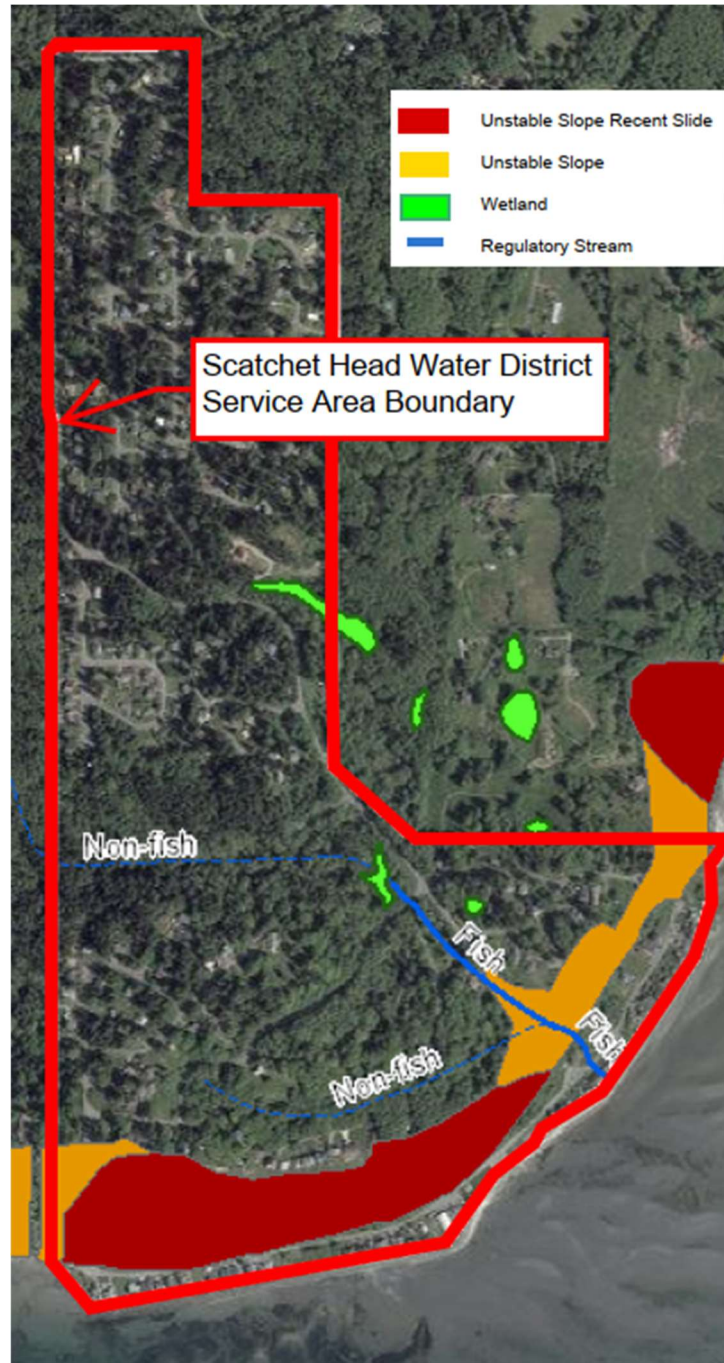


Figure 3: Sensitive Areas Map

1.3 Population Trends

The SHWD serves 409 full-time residential connection and 1 commercial connection. With approximately 900 residents, there are about 2.2 residents per connection. There are 492 residential lots within the service area. Therefore, if all residential lots are developed, the population within the service area has the potential to increase to about 1,100 residents in the future.

1.4 Community Engagement

The SHWD engages the community in the project planning process by holding monthly committee meetings and seeking community feedback. The projects proposed in this report are also discussed in the Water District's 2020 Water System Plan. With the release of the Water System Plan, the community had the opportunity to provide feedback on the capital improvements proposed in this report.

The SHWD informs the community of the aging infrastructure within the system and informs the community of the maintenance and repair costs. When water shutoffs are required for repairs, the residences are notified either in person or by phone. The members of the community are aware of the need to replace aging and failing infrastructure, including the asbestos concrete (AC) water mains.

2. EXISTING FACILITIES

2.1 History

The Scatchet Head Water District is located at the south end of Whidbey Island between Useless Bay and Cultus Bay. The SHWD provides water for the Plat of Scatchet Head (1965) and Cottage Glenn PRD (1996). Construction for the water system began in 1958.

Well #1 was the first well to supply the system and was located on Driftwood Drive (Lot 22 of Block 15). This well was abandoned in 1996 due to poor water quality. The well casing has been cut off below grade and filled in accordance with the criteria outlined by the Washington Department of Ecology. Well #2 (DOE Tag #ABR417) was first installed in 1980 and is located southwest of the intersection of George Drive and Samish Court. With the poor water quality from Well #1 on Driftwood Drive, Well #3 (DOE Tag #ABW832) was installed in 1995 on the same parcel as Well #2. In 1997, a reservoir at Maple Point for storage and a new distribution lines were added to serve 26 new lots. The wells, reservoirs, pressure zones and other facilities are shown in Figure 4.

With the installation of Well #3, the SHWD undertook a significant upgrade to the distribution system in 1999. The upgrades consisted of the installation of a dedicated transmission main from Wells #2 and #3 to the reservoir located on Guemes Avenue along with associated electrical and control elements. At the same time a building was constructed on the Guemes Avenue reservoir parcel to provide water treatment, booster pumps, and other associated appurtenances to monitor and control the distribution system. The new booster pumps allowed the reservoir to provide additional useful storage to the system and increased operating pressures. With this increase in operating pressure to replacement pressure reducing valves were installed which allowed for the removal of two old storage tanks to be abandoned.

The SHWD currently has 410 connections to its water system. The number of DOH approved connections is 451 connections. There are currently no pending requests for connections or annexations to serve property outside of the service area.

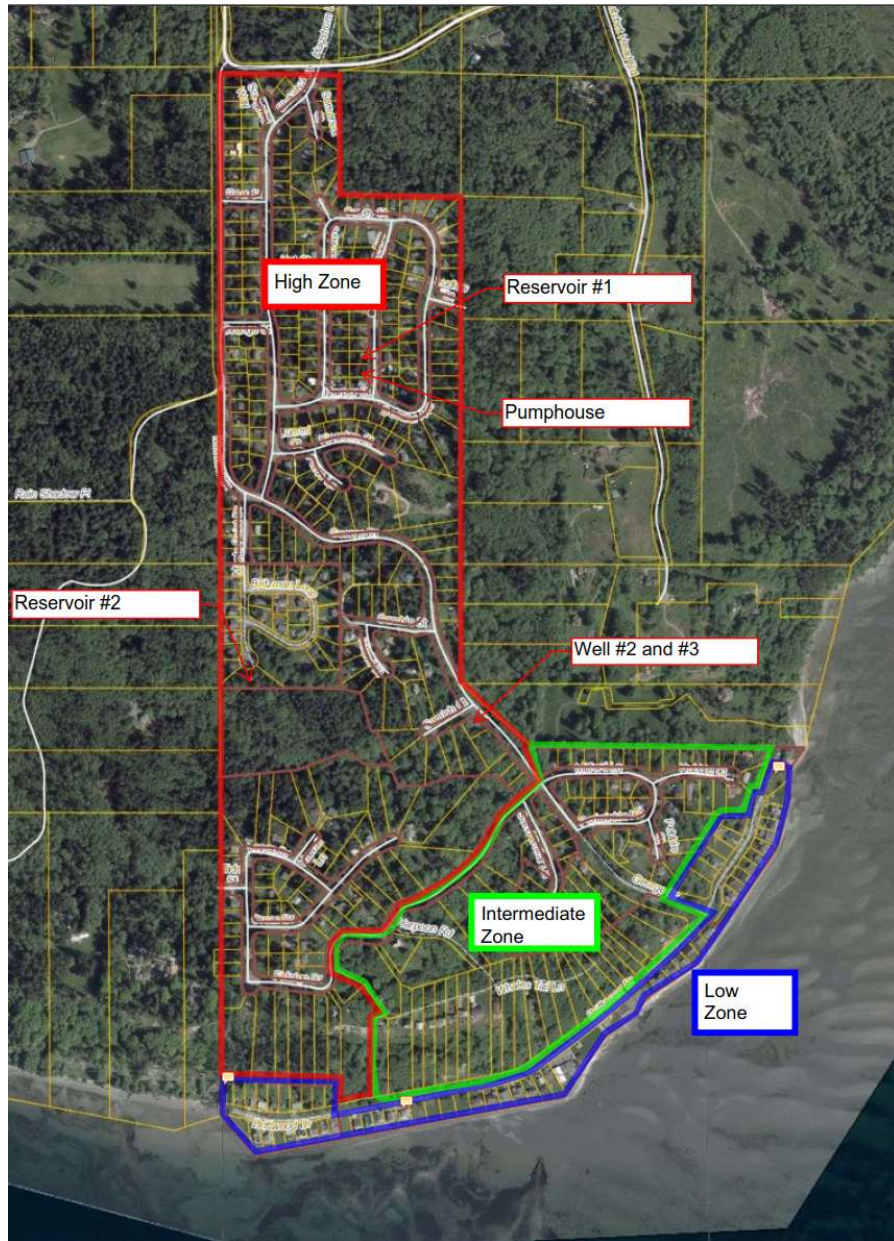


Figure 4: Pressure Zone and Facilities Map

2.2 Existing Conditions

2.2.1 Source:

The SHWD's distribution system is served by 2 groundwater wells. Both wells are located in parcel number S8110-00-12018-2. Well #2 has a capacity of 150 gpm and Well #3 has a capacity of 80 gpm (See the WFI in Appendix B). Both Wells #2 and #3 have pumps and meters that were installed in 1995 and 1997, respectively. Submersible well pumps and meters have an anticipated useful life of 10 to 15 years. Both the submersible well pumps and source meters and submersible well pumps are at or have surpassed their anticipated useful life and will need to be replaced.

In addition to the replacement of the source meter and submersible well pump, Well #3 has an undersized, 2-inch service line from the well to the pumphouse feed line. This 2-inch service line should be replaced with a 3- or 4-inch service line capable of conveying the full well capacity. Water quality data for each source is provided in Appendix F.

2.2.2 Storage:

There are two storage reservoirs in the system. Reservoir 1, located on Guemes Avenue, is a round steel reservoir with an inside diameter of 24.0-feet and a height of 85-feet with a total storage capacity of 300,000-gallons. Reservoir 2, located at the end of Maple Point Drive, has a diameter of 14.6-feet and a height of 95-feet and a total storage capacity of 120,000 gallons. Reservoirs 1 and 2 were installed in 1980 and 1997, respectively.

The existing reservoirs provide sufficient storage for the existing system demand. These reservoirs are projected to be adequate to serve the system through the projected 20-year planning period and are projected to provide at least 85% of the DOH-recommended standby storage. The only deficiency in the current storage is the ability to operate the system's booster pumps while Reservoir 1 is not in service. Piping configurations should be updated so that the system's booster pumps can still be operated while Reservoir 1 is not in service.

2.2.3 Booster Pumps, Pressure tanks, and Controls:

Four Aurora Series 340/360 7.5 hp booster pumps were installed in 1999 along with new booster pump controls. The other booster pumps appear to be functioning properly in accordance with system pressure settings. The booster pumps work in conjunction with a 2,120-gallon Canal Boiler Works pressure tank that was installed in 1980. Although it is aging, the pressure tank still functions properly and can hold pressure without any leaks. The only improvements to the booster system proposed in this project will be the modifications necessary to allow the distribution system to use the booster pumps while Reservoir 1 is not in service, as noted in Section 2.2.2.

2.2.4 Distribution System:

The system has a total of about 36,000-feet of distribution piping. The distribution piping consists of 4-inch, 6-inch, and 8-inch PVC piping, 6-inch AC piping, 6-inch and 8-inch ductile iron (DI) piping, and other 2-inch and 2½-inch piping. The larger PVC piping was primarily installed in 1996 and/or 1997. The AC, DI and other piping were installed in 1958. Distribution piping typically has an anticipated useful life of approximately 50-years. The AC piping is all over 60-years old and has been prone to leaks. This is a particular concern for the system since a 6-inch AC main down George Drive is the sole source of water for a significant number of houses in the southern portion of the system, including all of Driftwood Drive. It is recommended that the SHWD replace all the AC water mains within their distribution system.

There have been recent complaints from consumers regarding discoloration of water following recent repairs that were not satisfactorily addressed by flushing of the system. This is likely due to various parameters including various dead-end mains, improper placement of blow-off assemblies, pipe scale builds up in aging water mains, etc. When water mains are replaced, particular care should be given ensuring proper installation of pipes, placement of blow-off assemblies, and water mains should be looped to the extent possible.

The water main running north and south just west of Samish Court passes through a wetland area and is exposed, resting on wooden supports. This watermain should be prioritized for reburial or replacement, as necessary.

Currently, the system does not have fire hydrants located throughout the majority of the southern portion of the distribution system. There are various portions of the system with water mains that are insufficiently sized to provide the Island County's recommended residential fire flow rate of 500-gpm. Although the SHWD does not currently have plans to expand the service area, it would like to have the ability to serve all structures within the retain service area with hydrants capable of providing the recommended fire flow capacities. Water mains that are replaced should be sized to provide current and future demands, including residential fire flow. Hydrants should be located along the replaced water mains in accordance with Island County standards to serve structures in the service area to the extent that is particle.

2.2.5 Treatment/Pumphouse:

The system's pumphouse is located on the same property as Reservoir 1 on Guemes Avenue (Island County parcel S8110-00-05013-0). The pumphouse houses the booster pumps, pressure tanks, controls, and treatment system.

The treatment system was installed to reduce the elevated levels of iron and manganese in the system's source water. The treatment system consists of pre-chlorination, aeration, contact time in retention vessel (contact tank) and pressure filtration utilizing Birm® media. The treatment system was designed to reduce levels of iron and manganese to less than 50% of the Maximum Contaminant Level (MCL). The pre-chlorination is provided to mitigate the fouling of the treatment media by iron and sulfate-reducing bacteria. Following treatment, treated water is discharged directly to the top of the adjacent 300,000-gallon reservoir. The chlorinator and filtration system were installed in 2001. These systems typically have a life expectancy of about 30 years. The treatment system currently provides sufficient disinfection and has capacity to meet the current demands through the initial planning period. Filters are individually backwashed with backwash water discharged into a storage pond located directly adjacent to the pumphouse. The storage pond water is used to irrigate the lawn of the neighboring parcel since the lot's soils do not provide sufficient infiltration capabilities.

The treatment system's filter backwash rate is about 15%, which is higher than what would be anticipated from similar systems. This excessive backwash rate is indicative of an inefficient filtration process. The filter media has not been replaced since the original installation and is past its anticipated useful life. Well #3 in the system has had high arsenic values but is being mixed with Well #2 to keep system values under the MCL. It is anticipated that the proposed improvement will not have sufficient funds to address arsenic treatment. At a minimum, the filter process should be analyzed to ensure proper dosing and backwash and the filter media should be replaced.

The pumphouse has experienced leaking and a deterioration of the ductile iron piping within the building in the past few years. The chlorine storage tank is currently kept too close to the piping and accelerates the oxidation process. The corroded piping needs to be replaced, and the chlorine storage tank needs to be moved to a new location where it will be sealed off from the ductile iron piping and proper ventilation provided.

As it is currently configured, the filter-backwash process is pressurized from the booster pumps located within the pumphouse. However, as noted above, in the event that Reservoir 1 is taken offline for maintenance or repairs, the booster pumps are unable to function since the booster pumps are fed from Reservoir 1. In these circumstances the treatment system is taken offline until the reservoir is back in service. An analysis should be performed to determine if a piping configuration can be developed to allow booster pumps system to function while Reservoir 1 is not in use.

2.3 Financial Status of Any Existing Facilities

The expenditures and incomes for the SHWD have been compiled and outlined in Table 1 below. Detailed financial data are available in Appendix D.

Table 1: SHWD Expenditures and Income for 2016, 2017, 2018 and 2020

| Year | Total Expenses | Total Income | Net Income |
|---|----------------|--------------|------------|
| 2016 | \$127,881 | \$134,910 | \$7,029 |
| 2017 | \$136,574 | \$141,442 | \$4,867 |
| 2018 | \$150,344 | \$137,334 | -\$13,011 |
| 2020 (anticipated expenses & income) | \$117,150 | \$170,900 | \$53,750 |

In 2016 and 2017, the SHWD had a net positive income of about \$7,000 and \$4,900. However, in the year 2018, there was a net deficit of \$13,000. In 2019 and 2020 the SHWD updated their comprehensive Water System Plan with the Washington Department of Health. With the update, the system’s financial data was analyzed in conjunction with the anticipated Capital Improvement needs for the system. Due to this analysis, the SHWD implemented a revised rate structure with the intent of funding system needs into the future. In 2020, the SHWD is expected to have a net surplus of about \$54,000 due to increased water rates starting in 2020.

Detailed financial sheets are included in Appendix D of this report. An engineer’s preliminary construction cost estimate was completed and shows that the proposed system upgrades would cost approximately \$3,070,000 (see Appendix D). The SHWD is currently in the process of finalizing an interim loan to pay for the upfront costs associated with design and contract development prior to approval of the USDA Rural Development loan. This report has been prepared for application to the USDA Rural Development Program to acquire the needed funding to complete this project.

2.4 Water/Energy/Waste Audits

The most recent Water Efficiency Reports submitted to the Washington State Department of Health (DOH) are included in Appendix E of this report. The system is 100% metered. The reported average Distribution System Leakage (DSL) in 2019 was 14.1%.

The SHWD is designated as a group A Community Water System by the DOH. Using data from the 2019 Water Use Efficiency Report, the ADD (average day demand) was found to be 139 gpd/ERU. The ADD is consistent with other residential communities on Whidbey Island.

3. NEED FOR PROJECT

3.1 Health, Sanitation and Security

In the existing conditions, the SHWD is at risk of failed water mains, well pumps and other aging infrastructure. This presents a health risk from potential intrusion of contaminated surface water or back siphoning from the higher service connections. If a watermain breaks, a depressurization event will occur, presenting a cross-contamination risk throughout the system. Additionally, each break provides a point of entry for foreign contaminants to enter the system.

3.2 Aging Infrastructure

As frequently occurs with small systems, the system has been operated for an extended period without a proper plan in place for replacing and updating the aging infrastructure. Much of the system components are at or are nearing the end of their useful life. It is known that the distribution system has lost significant water in the past few years, which is characteristic of deteriorating infrastructure. There are several residences with aging water mains that are only served by dead-end mains. Therefore, if one of these watermains breaks and has to be taken out of service, all homes that are served by that main will have no water service until repairs can be made.

Neither of the well pumps have been serviced in more than 20 years. There is a risk of one or both well pumps failing. If this occurs, there will be a water outage for the entire system and the customers will have to rely on standby storage until reparations are made.

3.3 Fire Flow

Island County requires that new or expanding Group A residential system be capable of delivering fire flow at 500-gpm for 30 minutes with a minimum pressure of 20-psi at all locations, with the largest pump out of service. This would require at least 15,000 gallons of fire suppression storage in addition to the other required storage components including operational, equalizing, and dead storage. The existing reservoirs have a nominal storage volume of 420,000 gallons and can provide the necessary storage for fire flow.

Currently, the system is configured with four 7.5 HP Aurora Series 340/360 booster pumps, each of which is capable of providing approximately 220-gpm. DOH standards require that system be evaluated for fire flow with the largest pump out of service while the system supplies MDD. With one of the four operating booster pumps out of service, the three remaining pumps can provide 660-gpm combined, which is in compliance with DOH standards.

Several areas within existing system have 2-inch- and 4-inch watermains and are not capable of supplying 500-gpm without excessive loss of pressure. Generally, a minimum of 6-inch piping is necessary to allow for MDD and fire flow demand. Where water mains are replaced lines should be sized to allow for fire flow demand and hydrants should be installed or replaced as necessary to service structures.

3.4 Reasonable Growth

The SHWD currently has 410 connections to its water system and, with the updated Water System Plan, has been determined to be adequate to serve 597 equivalent residential units (ERUs). There is a total of 492 lots within the service area boundary with no current plans to expand the retail service area.

4. ALTERNATIVES CONSIDERED

4.1 No Action

The system could attempt to maintain the existing water mains and continue to repair leaks as they occur. Each repair represents a loss of service and potential contamination event. This does not provide the reliable level of service that is required by the DOH, due to the potential health concerns. In addition, it is anticipated that these problems will become exacerbated over time as the water mains age. Many of the existing pipes are beyond their useful life. Continued corrosion of the ductile iron piping in the pumphouse piping is no longer sustainable. Piping is already failing and being replaced as needed. Allowing the piping to fail will increase outages, degrade other infrastructure, and provide increased potential for contamination of the water in the distribution system. If the system continues to use the well pumps without replacing them, they will eventually fail and will have to be taken offline until an emergency replacement can occur.

In the year 2018, the SHWD spent about \$17,500 on repairs and maintenance. If no improvements are made to the system, the cost of maintenance and repairs is estimated to be about \$18,000 per year and will likely continue to increase significantly over time because of the aging infrastructure. If any emergency repairs or replacement need to occur, the cost of repairs and maintenance will likely increase significantly.

4.2 Distribution System Improvement Alternatives

Several potential improvements to the distribution system were considered. It is the intention of the SHWD to include as many of the AC water mains for replacement as is financially feasible. System as-builts for system have been analyzed to identify those AC water main over 60 years old that should be replaced as a major component of their system improvements. Several alternatives were considered for the repair or replacement of the aging water main including standard watermain replacement and trenchless water main replacement options such as slip-lining, cured in place pipe (CIPP), and pipe bursting. The improvement alternatives and descriptions are summarized in Table 2.

Various water mains are optional projects depending on available funding. Orcas Drive, Lopez Drive, and Fidalgo Drive are all insufficiently sized for residential fire flow. Fidalgo Drive, east of Harpoon Lane, has had issues with landslide in the past. If this line is replaced it, HDPE pipe should be used for its increased durability and flexibility. This location could potentially be an option for pipe bursting as discussed in the sections below.

The water mains through Mitford Lane, Pebble Court, and Periwinkle Road are insufficiently sized and have experienced continued issues with discolored water. These lines should be replaced and should loop back into the proposed water main on George Drive. Particular care should be given to minimize isolated low points during installation. A blow-off assembly should be installed at any isolated low spot for system maintenance.

Table 2: Distribution Improvement

| Street | Length | Existing Size/Type | Proposed Size/Type |
|------------------------------|----------|--------------------|--------------------|
| Blakely Avenue | 725-ft | 4" AC | 6" PVC |
| | 1,010-ft | 6" AC | 6" PVC |
| Pear Street | 215-ft | 4" AC | 6" PVC |
| Hat Street | 310-ft | 6" AC | 6" PVC |
| San Juan Avenue | 230-ft | 6" AC | 6" PVC |
| Casey Street | 340-ft | 6" AC | 6" PVC |
| Guemes Avenue | 730-ft | 6" AC | 6" PVC |
| Harper Street | 530-ft | 6" AC | 6" PVC |
| George Drive | 3,720-ft | 6" AC | 8" PVC * |
| Mitford Lane | 710-ft | 2" PVC | 6" PVC |
| Pebble Court/Periwinkle Road | 640-ft | 2" PVC | 6" PVC |
| Harpoon Lane | 670-ft | 4" AC | 6" PVC |
| Driftwood Drive | 1,620-ft | 4" AC | 6" PVC |
| | 1,230-ft | 6" AC | 6" PVC |
| OPTIONAL SECTIONS | | | |
| Hubble Court | 370-ft | 2" PVC | 6" PVC |
| Orcas Drive | 505-ft | 4" PVC | 6" PVC |
| Lopez Drive | 290-ft | 4" PVC | 6" PVC |
| Driftwood Drive | 625-ft | 2" PVC | 6" PVC |
| Fidalgo Drive | 915-ft | 4" PVC | 6" HDPE |
| | 1,210-ft | 4" AC | 6" HDPE |

* The watermain down George could potentially be an 8" HDPE line depending on system configurations

A map of the proposed water main replacements is provided in APPENDIX A.

4.2.1 Trenchless Installation Options

The following sections discuss means and methods of replacing water mains through trenchless installation methods. These methods all involve some trenching to access mains and connections and were evaluated for applicability for the main replacements proposed by SHWD.

4.2.1.1 Slip-Lining Water Mains

Slip-lining involves threading a smaller pipe through the existing water main pipe. The annular space between the new pipe and existing main is then sealed with a grout so that they act as a single pipe. As with other trenchless technologies, slip-lining, has the benefit of allowing the installation of new pipe without the need for extensive trenching. This process can be particularly beneficial though sensitive areas and where there are conflicts with other utilities.

Consideration should be given to the installation process. The process will require the existing water main to be out of service throughout installation, testing, and reconnection of the services and to the existing system. Although trenching is reduced, it is still necessary to open the main at each service connection, tee, cross, and at some fittings. Also, the resulting pipe size is smaller and will provide less capacity which can negatively impact system efficiency. All these factors should be considered with the potential selection of slip-lining as an installation method.

4.2.1.2 Cured in Place Pipe (CIPP)

CIPP consists of installing a flexible liner into the existing water main. The liner is embedded with epoxy and resin so that the system can be sealed and pressurized with hot air. The process of pressurizing with hot air allows the liner to conform to the existing pipe shape and hardens the liner in that process. The installed liner is thin allowing the water main to maintain a similar capacity.

Consideration should be given to the process and limitations presented with CIPP installation. The lining does not conform well to fitting in a system. Therefore, access to the water main is required at all fittings and service connections to allow for other connections. During this process, the existing main will be out of service affecting all service connections off of that line or dependent on that section of main. This process is most efficient on straight uninterrupted section of water main. Cost benefits occur from avoiding disturbances to critical areas, pavement, adjacent utilities, and structures.

4.2.1.3 Pipe Bursting

Pipe-bursting involves pulling or pushing a new pipe through the existing water main with a pipe bursting head. The bursting head is pulled through the existing main via a hydraulic. As it is pulled back through, the blades on the bursting head cut apart the existing pipe. An expander head then follows and pushes the pipe fragments out into the surrounding soil. Following this expander, a new pipe is pulled into place in the space once occupied by the original pipe.

As with the other trenchless technologies discussed above, pipe bursting requires access to the existing main at all crossing, and service connections. Customer connections off the section of pipe will be affected as will other sections of pipe dependent of repaired sections.

4.2.1.4 Trenchless Installation Conclusions

These methods of pipe repair/replacement are advantageous in that they do not involve trenching and digging. Cost benefits arise from avoiding redesign due to avoiding critical areas, minimizing impact the pavement and other structures, avoiding impacts to other utilities, and delays from unforeseen obstacles that can occur with open trenching.

However, each method discussed requires that the existing mains be shut down during the entirety of the construction process. This will leave the connections off the repaired water main, or connections dependent on that section of water main, without water during mobilization, installation, curing, testing, and reconnection of the system. At times, overground lines can be run to serve various connections, but the is only recommended for short distances that can be typically be accessed from hydrants. Although trenching is reduced it will still be necessary to access the existing main at all tees, service connections, hydrants, and at some fittings.

The current system has extensive sections of system that are dependent on a single water main due to the lack of loops in the system. This reduces the efficiency of the trenchless solutions since it would be cost prohibitive to prove a significant number of connections with water throughout the installation and testing process. Due to the location of water mains outside of asphalt, except at crossing, and limited conflicts with existing utilities, many of the benefits of trenchless installation are nullified. It is anticipated that the most efficient and cost effective means of water main replacement, in most cases, will be to install a new line via open cut processes so that the existing services can be maintained until reconnection to the new water main is prepared and approved. The exceptions to this is the portion of Fidalgo Drive between Harpoon Lane and George Drive. This section of pipe has no services and passes

through a critical slope. Pipe bursting should be considered for this location. If pipe bursting is used, it is recommended to increase the water main size to 8" HDPE.

4.3 Pressure Reducing Valves

The SHWD is also planning on replacing and relocating the Pressure Reducing Valve (PRV) stations located on the water mains to maintain system pressures within the recommended values set by the DOH. The configuration of the system will mimic the existing pressures zones that exist in the current system with some potential minor modifications dependent on the improvements along Fidalgo Drive.

A PRV station will be located on George Dr close to Fidalgo Dr. There is an existing PRV on Fidalgo Drive that will be relocated with the proposed water main improvements to improve the functionality and service along Mitford Lane, Hubble Court and Periwinkle Road.

The PRV station at Harpoon Lane will be replaced with the waterline improvements. The location of the PRV station could be relocated to the intersection with Whales Tail Lane depending on available space and access issues.

The PRV station located at the intersection of Driftwood Drive and George Drive was installed in 2007 and appears to be in good condition. Improvements along Driftwood Drive will connect into this existing PRV vault.

An alternative to the PRV on George Dr that was considered is the installation of PRVs on each residence served on Mitford Ln. This option, however, was not selected because the installation cost is greater, and the pressure would only be reduced for the service lines, not the mains. The water mains would also remain at higher pressures which could be detrimental to the system.

4.4 System Loops and

Depending on available funds there are some additional loops that should be considered to improve water movement in the distribution system. Currently Driftwood Drive is only served by the water main down George Drive. It would be advisable to have a second source of water to these residences. Similarly, Mitford Lane and the streets connected to it will also only be served by the water main down George Drive if the line down Fidalgo Drive is abandoned at Harpoon Lane.

Various options were considered to loop Driftwood Dr. In Option A, a water main would be added to connect Hubble Court to the north end of the main along Driftwood Drive. A PRV station would be added to Hubble Court to reduce pressures going down to Driftwood Drive. This would require the installation of a line through a critical slope. Installation of a water main in this located should be installed by directional drilling to avoid impacts to the slope. HDPE pipe should be used due to its durability, fused connections, and flexibility. This option includes the optional replacement of water mains along Hubble Court and the 2-inch PVC on Driftwood Drive. Option B would be to install a new line by directionally drilling from the end of Whales Tail Lane to a point on the western portion of Driftwood Drive. This option would also require the installation of a PRV station and the replacement of water mains on Whales Tail Lane. to provide adequate flow. Option A is more cost effective and would also remove the dead-end line on the north end of Driftwood Drive. However, it is advisable to install one of the two options, if funds are available, in order provide an additional source of water to Driftwood Drive and to reduce the stagnation of water in the dead ends of those portions of the distribution system.

4.5 Exposed Piping

The water main running north and south just west of Samish Court is passing through a wetland area and is exposed, resting on wooden supports. It is advisable to bury this section of pipe to protect it from debris and potential impacts. Alternatively, work could be undertaken to encase the pipe and replace the pipe supports.

4.6 Pumphouse and Treatment Improvements

The pumphouse and treatment system are at the core of the distribution system. The system required various improvements to address existing system problems as discussed in previous sections. Those deficiencies are discussed in greater detail in the sections below.

4.6.1 Treatment System Improvements

The treatment system has an abnormally high backwash rate and has experienced disinfection byproducts in the past. Both issues are indicative of inefficient treatment. In addition, the treatment system was originally designed with alternate forms of oxidation which has been replaced due to its ineffectiveness. The treatment system should be analyzed to determine the cause of these issues. The filter bedding, which was originally designed to be compatible with ozone treatment, will likely need to be replaced and upgraded with an improved filter media. The filters currently have Birm® media filter bedding which was installed in 2001. One alternative that was considered is replacing the existing filter media with Greensand Plus®. At a minimum, the filter media should be replaced, dosing rates and oxidation methods should be analyzing to improve the efficiency of the system in removing iron and manganese. A thorough analysis of the system should be done to diagnose the cause of the issues. Another improvement alternative is to replace the entire filtration system with a new ATEC® filter system which could be designed to treat and remove arsenic that is also present in Well #2. Any improvements to the treatment system should, at a minimum, be designed to match the instantaneous water right of the SHWD. Due to the age of the current system and the anticipated age at the time of completion this improvement will be scoped for a full replacement of the treatment system. A full improvement can have the added benefit of modifying the backwash method as discussed below.

4.6.2 Disposal of Backwash Water

The SHWD currently uses a pond to store backwash water. The backwash pond is metered out with a separate pump and used for irrigation of Island County parcel S8110-00-05014-0. Using the backwash water for irrigation works well during the dry season, but it is not ideal during the wet season as the ground is often already saturated, causing excess water to flow back into the pond for continued use. Alternative methods of disposal should be considered for the backwash water. The option that is being considered is discharging the backwash water into the roadside ditch on the east side of Guemes Avenue. The ditch conveys water to the south, east and then north following Decatur Avenue. An Island County outfall conveys stormwater from the roadside ditch in Decatur Avenue into a natural ravine located along the east edge of the Scatchet Head Plat. Any potential improvements would need to ensure a properly sized drainage path to ensure that there will not be adverse impacts to neighboring properties.

4.6.3 Configuration to Serve Booster Pumps

As it is currently configured, the filter-backwash process is pressurized from the booster pumps located within the pumphouse. However, as noted previously in this report, in the event that Reservoir 1 is taken offline for maintenance or repairs, the booster pumps will be unable to function because they are fed from Reservoir 1. In these circumstances, the treatment system is taken offline until the reservoir is

back in service. An analysis should be performed to determine if a piping configuration can be developed to allow booster pumps system to function while Reservoir 1 is not in use. There are various options that could be considered.

An option would be to feed the booster pumps directly from the dedicated raw water line. This option would require gate valves to reroute raw water from the filter process into the suction line of the booster pumps. A check valve would be installed to ensure water is not pressurized back toward the wells. This option would also not allow for the use of the treatment system while Reservoir 1 is out of service.

Another option would be to backwash the filters from the raw water wells. This would require reconfiguration of the piping in the pumphouse to direct raw water from the wells through the backwash with a pressure sustaining valves. The design would need to ensure that the smaller capacity well would have a sufficient flowrate to properly backwash the filters.

4.6.4 Corroded Piping

The corroded ductile iron piping in the pumphouse needs to be replaced. The existing piping was designed and installed appropriately, however the chlorine tank is currently stored too close to the iron piping which accelerated the oxidation of several pipes. The chlorine tank will be relocated to a new ventilated storage room to avoid corrosion of the new piping. When this piping is replaced the necessary reconfiguration of the piping system to account for changes to the treatment system can be implemented.

4.7 Source Improvement

Both well pumps were last replaced approximately 20-years ago. It is essential that both well pumps be replaced. No other alternatives to pump replacement were considered. When the well pumps are replaced, the meters will also be replaced along with any piping that is undersized for the associated well capacity.

The well pumps are not able to function when there are power outages on the system. During these times, the SHWD attempts to limit consumption so that the system can be served by its available standby storage. System pressures are maintained by the booster pumps which can be powered by a backup generator. To improve the District's emergency preparedness, an emergency generator should be installed to power the well pumps in the event of an extended power outage or other emergency. Installation of an emergency storage tank of 5,000 gallons can also be installed on the well site to provide a source of potable water for residents in an emergency event where the distribution system is significantly compromised.

5. SELECTION OF AN ALTERNATIVE

The costs associated with the various alternatives for repairing the aging infrastructure at Scatchet Head Water District are summarized in **Error! Reference source not found.** Detailed preliminary cost estimates are included in Appendix D. The combined capital cost of all proposed improvements is expected to be about \$2,590,000.

Table 3: Improvement Alternatives – Cost Estimate Summary

| Category | Alternatives | Capital Costs | Lifespan (years) | Annual O&M Cost |
|-----------------------|---|---------------|------------------|-----------------|
| Distribution | 1) Open Trench Replacement | \$2,810,000 | 60 | \$5,000 |
| | 2) Pipe Bursting | \$5,220,000 | 60 | \$5,000 |
| | 3) Cured in Place Pipe | \$4,920,000 | 60 | \$5,000 |
| | 4) Do Nothing | \$0 | n/a | \$20,000 |
| Pumphouse & Treatment | 1) Improvements with Greensand® Plus Filter Bedding | \$40,000 | 15-20 | \$20,000 |
| | 2) Improvements with New ATEC® Filtration System | \$140,000 | 15-20 | \$4,800 |
| Source | 1) Well pump, piping, and meter replacement | \$80,000 | 15-20 | \$4,800 |

As noted previously, it was determined that standard open trench installation of new water mains would be the best, in most cases, due to lower costs and the ability to maintain water service to most of the SHWD’s consumers. The water main replacements will also include the replacement of any fire hydrants off those water mains and the placement of additional hydrants where adequate flows can be provided. New dedicated sampling stations will be located to provide for necessary system testing and maintenance and any meters located in the back of parcels will be relocated to the right-of-way to allow for improved access and maintenance with accordance with system standards. Preliminary schematic drawings of the proposed improvements are included in Appendix A.

For pumphouse and treatment improvements it is anticipated that the full replacement of the treatment system will be most beneficial to the long-term maintenance of the facility. The ability to properly size the filter vessels for use with backwash from the wells, improved media, and the ability to provide treatment for arsenic will improve the system functions with the benefits of low-cost future maintenance. Chlorine and any other chemicals used in the treatment process will be relocated to a new storage room with proper ventilation to protect pumphouse piping and infrastructure from corrosion. Details of the proposed improvements are included in Appendix A.

The source improvements will consist of replacing the well pumps, some of the piping, and the source meters, as well as installation of an emergency generator, and a 5,000-gallon emergency storage tank as detailed in Appendix A.

5.1 Life Cycle Cost Analysis

The cost for the various alternatives were analyzed for the present worth to aid in determination of an appropriate alternative. A life cycle cost analysis was performed and is included with Appendix D. Results are presented below in **Error! Reference source not found.** The present values were calculated assuming an inflation rate of 1.5%/yr.

Table 4: Net Present Value

| Category | Alternatives | Capital Costs | Inflation Rate | Net Present Value |
|-----------------------|---|---------------|----------------|-------------------|
| Distribution | 1) Open Trench Replacement | \$2,810,000 | 2.5% | \$2,965,000 |
| | 2) Pipe Bursting | \$5,220,000 | 2.5% | \$5,375,000 |
| | 3) Cured in Place Pipe | \$4,920,000 | 2.5% | \$5,075,000 |
| | 4) Do Nothing | \$0 | 2.5% | \$618,000 |
| Pumphouse & Treatment | 1) Improvements with Greensand® Plus Filter Bedding | \$40,000 | 2.5% | \$99,000 |
| | 2) Improvements with New ATEC® Filtration System | \$140,000 | 2.5% | \$199,000 |
| Source | 1) Well pump, piping, and meter replacement | \$80,000 | 2.5% | \$96,000 |

6. PROPOSED PROJECT

6.1 Preliminary Project Design

Bentley WaterCAD was used to create a hydraulic model of the preliminary design of the proposed distribution system. Three scenarios were modelled: Scenario 1 included no water demand and the high pressure setting, Scenario 2 modelled the system at PHD and the low pressure setting, and Scenario 3 modelled fire-flow at MDD. Model results are summarized below. Detailed results can be found in Appendix G.

Scenario 1 modelled the high-pressure scenario where there is no demand on the system, and the pressure at the booster pump station is set to 55-psi, which is the high setting of the booster pumps. This scenario resulted in pressures ranging from 40-psi to 117-psi in the distribution system. However, at the residential service connections, the pressures range from 42 psi to 85-psi. The highest pressures that occur at service connections happen at the end of Hubble Ct. All other static water pressures at service connections are below 85-psi. These pressures will likely be the highest pressures that the system will experience during operation.

Scenario 2 modelled the system at a PHD of 297-gpm, which is the expected peak flow rate of the system in the with all 455 available lots using a connection. In this scenario, the pressure at the booster pump station was set to 45-psi. The pressures in the system ranged from 40-psi to 117-psi. The pressure of the mains at water service connections ranged from 41-psi to 104-psi. The highest pressures are located at the end of Samish Ct (104-psi), along Fidalgo Drive close to Harpoon Road (91-psi) and at the end of Hubble Court (85-psi). These high-pressure areas represent few potential connections which could be managed with individual PRVs. All other pressures at service connections were found to be below 80-psi.

Scenario 3 represents the system during fire-flow situation during MDD. The MDD that was used is 425 gpd/ERU, as found in the 2020 Water System Plan. In 20 years, the system is anticipated to have 455 connections, therefore the overall MDD of the system that was modelled was 193,375 gpd or 135-gpm. A demand of 500-gpm was also placed on the fire-hydrant at the highest elevation within the system

which is located along Blakely Avenue and Swede Hill Road. This scenario resulted in pressures in the distribution system that ranged from 39-psi to 114-psi.

All scenarios that were modelled produced acceptable results. The static-pressure scenario resulted pressures that were less than 90-psi for all but two service connections. The PHD scenario resulted pressures that met the 30-psi minimum requirement. And the fire-flow scenario showed that the distribution system is capable of conveying fire-flow without any pressures within the system dropping below 20-psi.

6.2 Project Schedule

The Scatchet Head Water District is currently submitting a preliminary engineering report for USDA Loan approval, and the loan review period is expected to take 3 to 4 months. Assuming the loan application is approved, the next step would be preparation and submittal of a project report to the Washington State Department of Health (DOH) for any projects not accounted for in the District's Water System Plan. This project report can be completed in conjunction with the development of construction documents, contract documents, and engineering specifications. The development of these documents is anticipated to take 4 to 5 months. Following the development and approval of relevant construction documents, the project will be publicly bid, a contractor selected, and construction contracts can be finalized. The public bid process through finalization of the construction contract typically is a 2 to 3 month process.

Project construction, testing, approval, and closeout procedures would follow contract approval and typically last an additional 4 months. The complete schedule estimate from November 2020 is approximately 15 to 18 months. The project could be expected to be completed in the first or second quarter of 2022.

6.3 Permit Needs

The following permits will be required to support the proposed work:

- The waterline installation will require a Permit to Work in the Right of Way from Island County Public Works.
- Additional easements may be needed from some homeowners
- A Clearing and Grading Permit may be required from Island County Planning (depending on total estimated combined cut and fill quantities).
- A Project Report outlining the proposed water system improvements will be submitted for approval to the Washington State DOH for any projects not addressed in the District's Water System Plan.

Any additional, relevant permits will be obtained by the selected contractor. The water system will need to obtain or update their Franchise agreement, if needed, prior to the start of Construction. The project is SEPA exempt since it involves replacing existing utilities.

6.4 Annual Operating Budget

The operational budget is provided in Appendix D and summarized in Table 1. The system currently receives income from water service fees, late fees, and reimbursed expenses. Residents are charged a base quarterly service charge and are charged water rates that are described in Table 3. The rates will be gradually increasing in the coming years as shown below.

Table 3: Increasing Block Rate Structure

| | 2019 | 2020 * | 2021 | 2022 |
|----------------------|---------|----------|----------|----------|
| Metered Connection** | \$94.52 | \$116.58 | \$142.31 | \$154.39 |
| 2,0000 -3,000 CF*** | \$0.070 | \$0.070 | \$0.070 | \$0.070 |
| Over 3,000 CF*** | \$0.090 | \$0.090 | \$0.090 | \$0.090 |

* Effective rate as of November 2020.

** Meter connection includes the cost for the first 2,000 cubic feet of water.

*** The cost shown is the cost of water per cubic foot of usage.

Annual expenditures are summarized in Table 1 and are laid out in Appendix D. In 2018, the total operating expenses were about \$150,000. The repairs and maintenance costs for 2018 were about \$17,500. After construction of the project described in this report, the costs for repairs and maintenance are expected to be reduced.

7. CONCLUSIONS AND RECOMMENDATIONS

The SHWD currently provides potable water to 410 connections within their service area in Clinton, WA. The system is obligated to provide reliable service to its customers and the proposed project will provide the infrastructure needed to deliver water in compliance with county, state, and federal requirements. Much of the distribution system was installed more than 50 years ago. The proposed project improvements will include replacing aging water mains, providing fire flow capacity throughout the distribution system, installing pipe supports for an exposed watermain, loop dead end watermains, and install a new PRV station. The project will also include improvements to the treatment system and sources such as upgrading the filter bedding, replacing corroded piping within the pumphouse, installing a new backwash water disposal location, adding a new ventilated storage room for the chlorine storage tank, replacing well pumps, piping and meters, and installing an emergency generator and storage tank. The proposed project will greatly improve system reliability and reduce contamination risk. The total project costs are expected to be approximately \$3,070,000.

APPENDIX A Maps and Schematics

Scatchet Head Water District



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Plats

Plat Existing Service Area

Parcels

Quarter Sections

One Way Directions

Road Closures

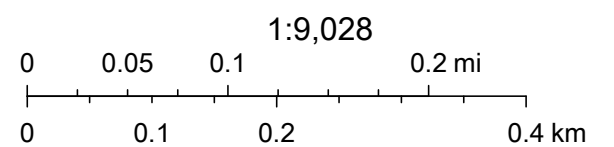
Roads

Highway

Collector and Arterial

Local

Private



Source: Esri, DigitalGlobe, GeoEye, Earthstar Geographics, CNES/Airbus DS, USDA, USGS, AeroGRID, IGN, and the GIS User Community
Island County

Proposed Distribution System Improvements

NOTES:

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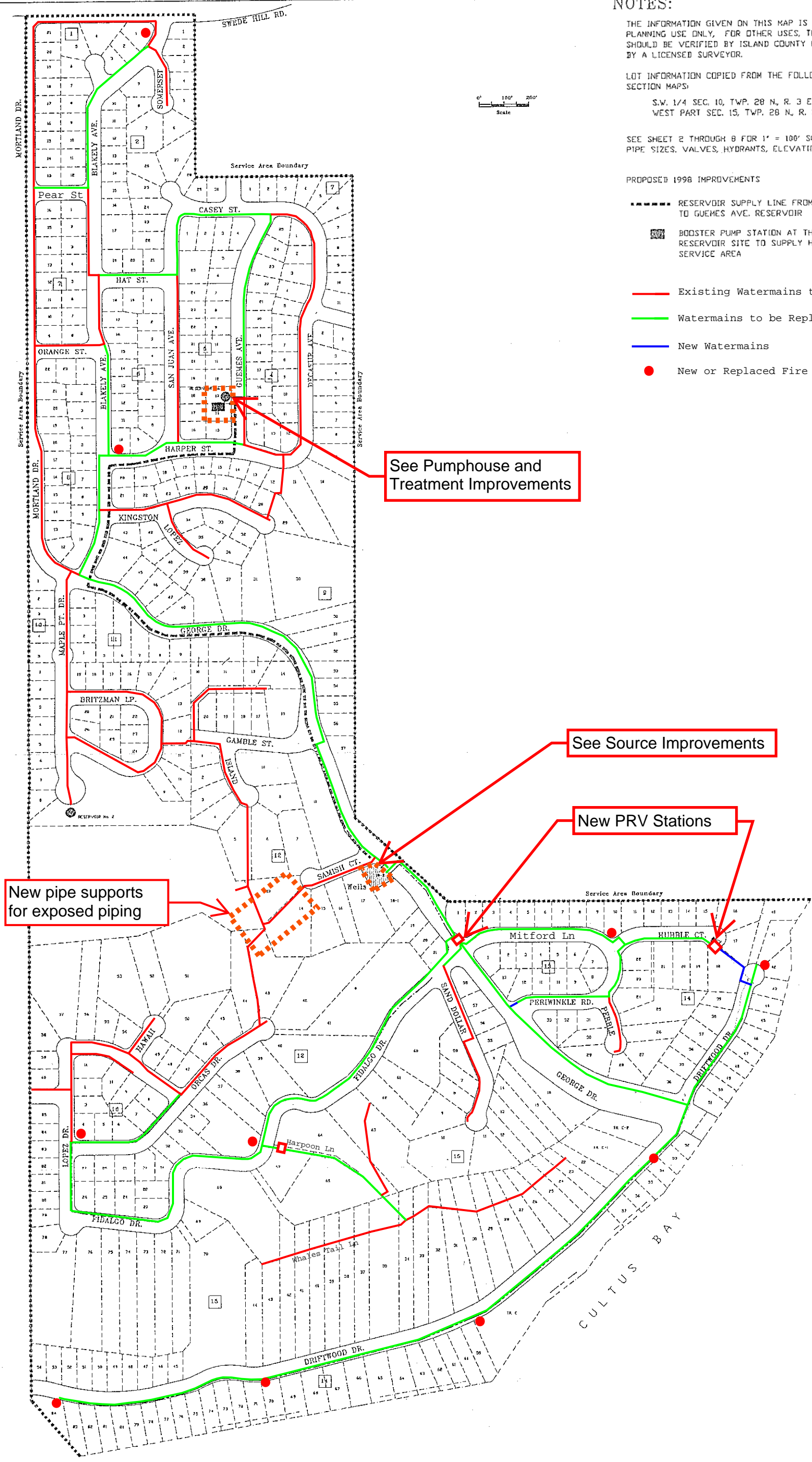
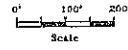
LOT INFORMATION COPIED FROM THE FOLLOWING ISLAND COUNTY SECTION MAPS:

S.W. 1/4 SEC. 10, TWP. 28 N., R. 3 E., W.M.
WEST PART SEC. 15, TWP. 28 N., R. 3 E., W.M.

SEE SHEET 2 THROUGH 8 FOR 1" = 100' SCALE PLANS SHOWING PIPE SIZES, VALVES, HYDRANTS, ELEVATION CONTOURS, ETC.

PROPOSED 1998 IMPROVEMENTS

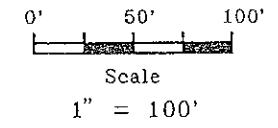
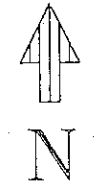
- RESERVOIR SUPPLY LINE FROM WELLS TO GUEMES AVE. RESERVOIR
- BOOSTER PUMP STATION AT THE GUEMES AVE. RESERVOIR SITE TO SUPPLY HIGH ELEVATION SERVICE AREA
- Existing Watermains to Remain
- Watermains to be Replaced
- New Watermains
- New or Replaced Fire Hydrant



LATEST REVISION: 1/27/98

SWEDE HILL RD.

6"φ C-900 PVC (1997)



Notes:

(COMMON TO ALL SHEETS)

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LOT INFORMATION COPIED FROM THE FOLLOWING ISLAND COUNTY SECTION MAPS:

S.W. 1/4 SEC. 10, TWP. 28 N., R. 3 E., W.M.
WEST PART SEC. 15, TWP. 28 N., R. 3 E., W.M.

Legend:

(COMMON TO ALL SHEETS)

- (W) Lot with active water service.
- w Lot with inactive water service
- Service area boundary
- Water main
- Water service
- Water service c/w shutoff and meter setter
- GV # Gate valve
- BO # Standpipe / Blow-off
- HYD # Fire hydrant (c/w isolating valves)
- AV # Air release valve
- WSS # Water sample station
- FC Field chlorine measurement at house tap by customer
- Pressure reducing valve in vault

- Proposed 6" PVC Watermain
- Proposed 8" HDPE Watermain
- New or Replaced Fire Hydrant

MORTLAND DR.

6"φ C-900 PVC (1997)

BLAKELY AVE.

6"φ C-900 PVC (1997)

CASEY ST.

6"φ AC (1958)

6"φ AC (1958)

6"φ AC (1958)

6"φ PVC (1997)

See Sht. 3

Latest Revision: 1/27/98

SCHAEFER & BRATTON, ENGINEERS
P. O. Box 607
Coupeville, Washington 98239
Job 297 November 1997

WATER DISTRIBUTION SYSTEM
COMPREHENSIVE MAP

SCATCHET HEAD WATER DISTRICT
3792 EAST HUBBLE COURT
Clinton, Washington 98236

Sht. 2 of 10

MORTLAND DR.

Service Area Boundary

6"φ PVC (19--)

6"φ PVC (19--)

VSS # 1

See Sht. 2

6"φ AC (19--)

HAT ST.

6"φ PVC (19--)

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GV 10

ORANGE ST.

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GV 2

6"φ AC (19--)

GV 13

GV 14

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HYD 6

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See Sht. 4

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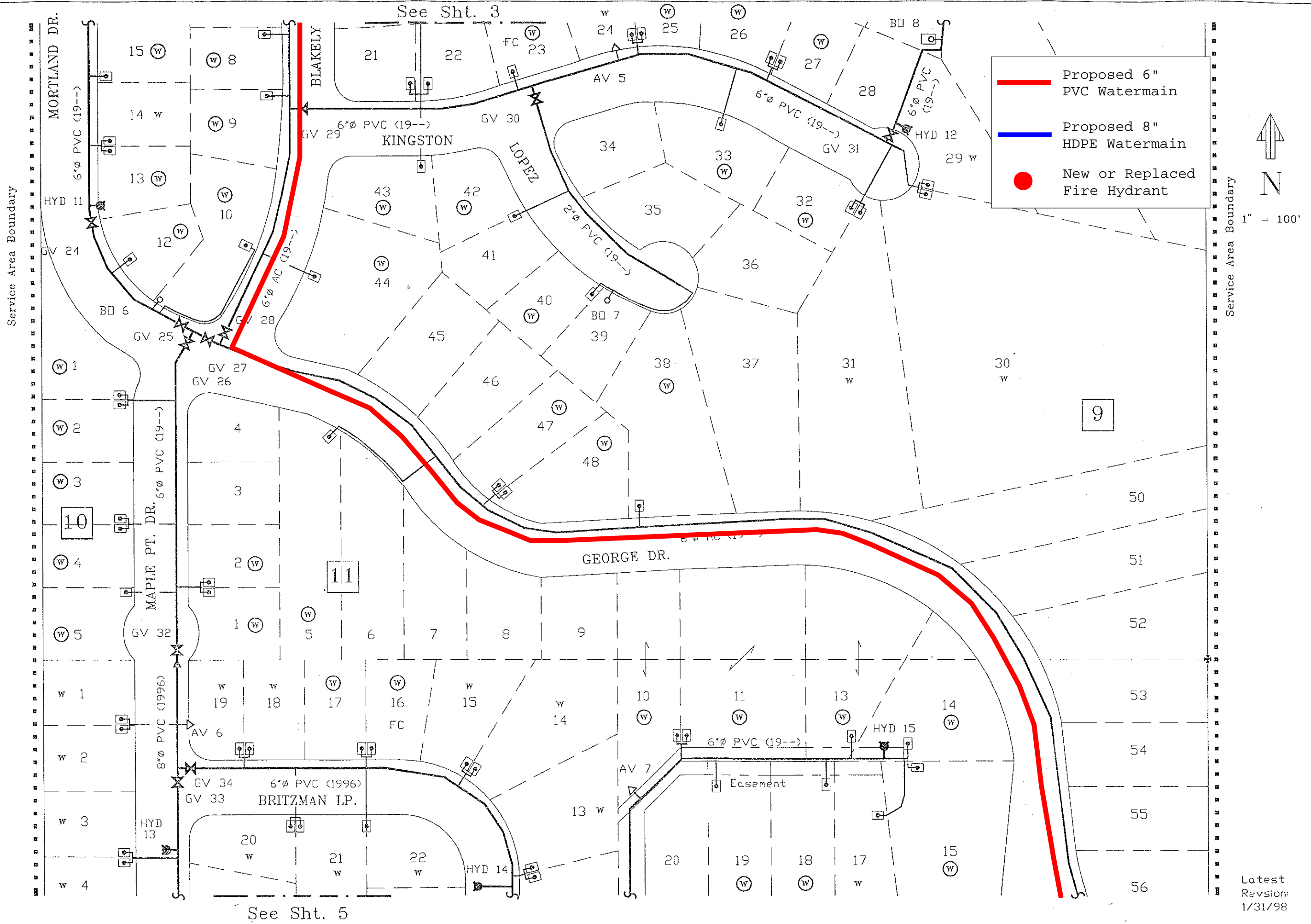
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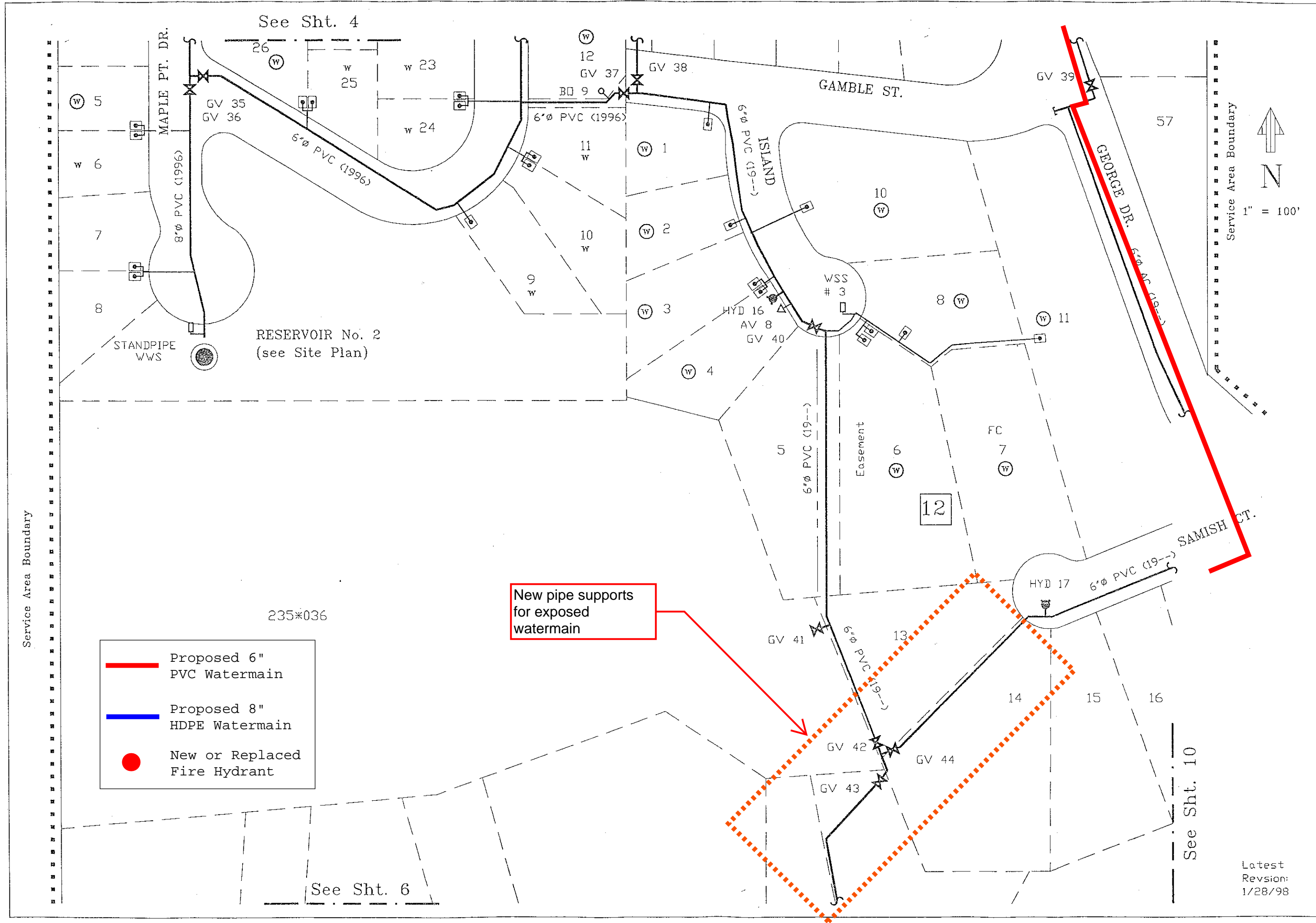


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 Job 297 November 1997

WATER DISTRIBUTION SYSTEM
 COMPREHENSIVE MAP

SCATCHET HEAD WATER DISTRICT
 3792 EAST HUBBLE COURT
 Clinton, Washington 98236

Latest Revision: 1/31/98

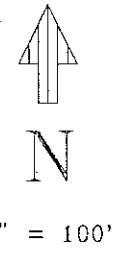


See Sht. 4

RESERVOIR No. 2
(see Site Plan)

New pipe supports
for exposed
watermain

- Proposed 6" PVC Watermain
- Proposed 8" HDPE Watermain
- New or Replaced Fire Hydrant



See Sht. 6

See Sht. 10

Latest
Revision:
1/28/98

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Job 297 November 1997

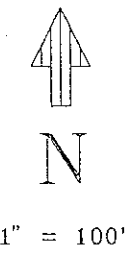
WATER DISTRIBUTION SYSTEM,
COMPREHENSIVE MAP

SCATCHET HEAD WATER DISTRICT
3792 EAST HUBBLE COURT
Clinton, Washington 98236

Service Area Boundary

See Sht. 5

See Sht. 10



Proposed 6" PVC Watermain

Proposed 6" HDPE Watermain

New or Replaced Fire Hydrant

Option A - Fire Flow to Lopez & Harpoon

Option C - Fidalgo Loop

New PRV

Option A - Fire Flow to Lopez & Harpoon

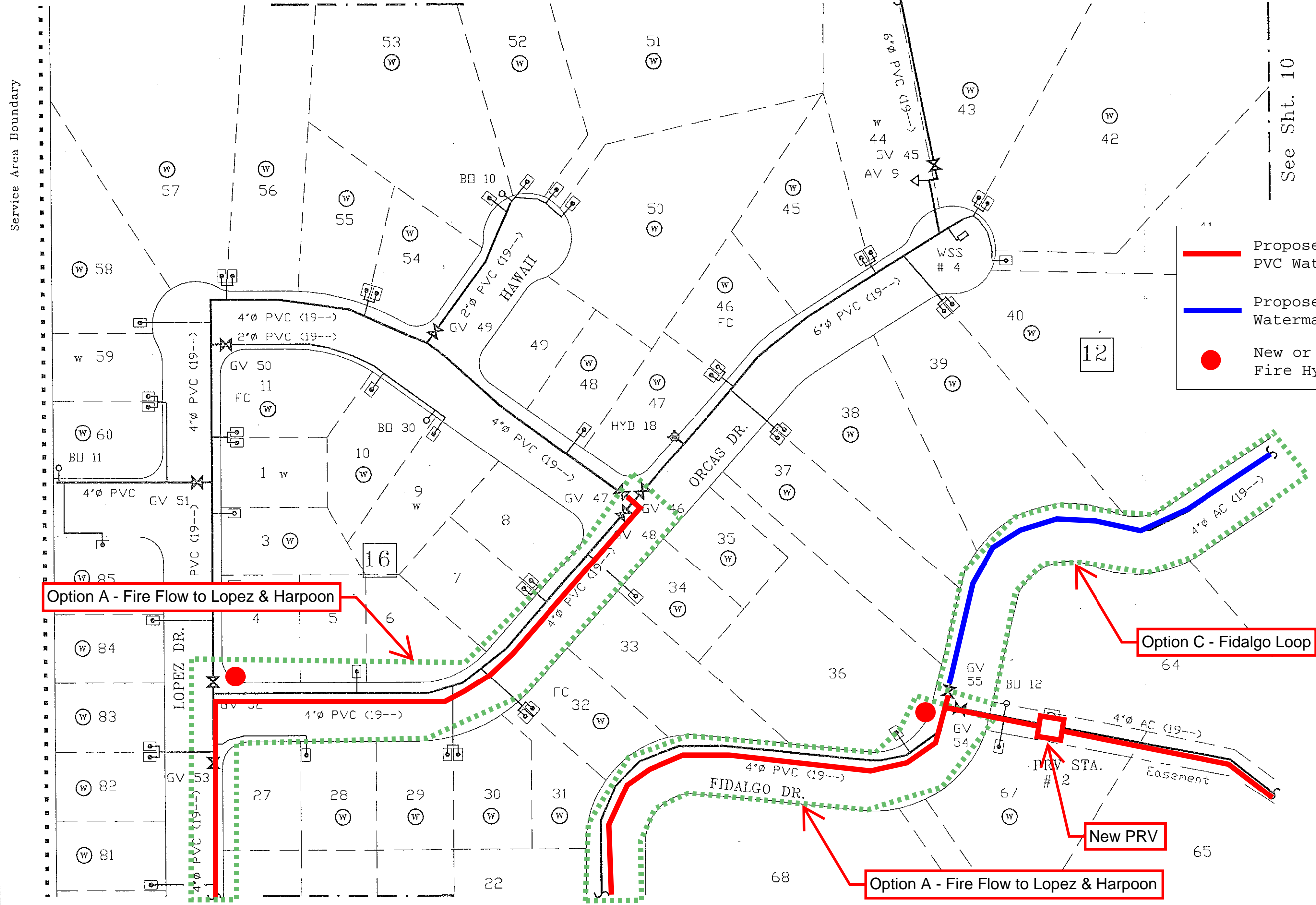
Latest Revision: 1/31/98

SCHAEFER & BRATTON, ENGINEERS
P. O. Box 607
Coupeville, Washington 98239
Job 297 November 1997

WATER DISTRIBUTION SYSTEM
COMPREHENSIVE MAP

SCATCHEL HEAD WATER DISTRICT
3792 EAST HUBBLE COURT
Clinton, Washington 98236




Sht. 6 of 10



Service Area Boundary

See Sht. 6

Option A - Fire Flow to Lopez & Harpoon

-  Proposed 6" PVC Watermain
-  Proposed 8" HDPE Watermain
-  New or Replaced Fire Hydrant

See Sht. 8

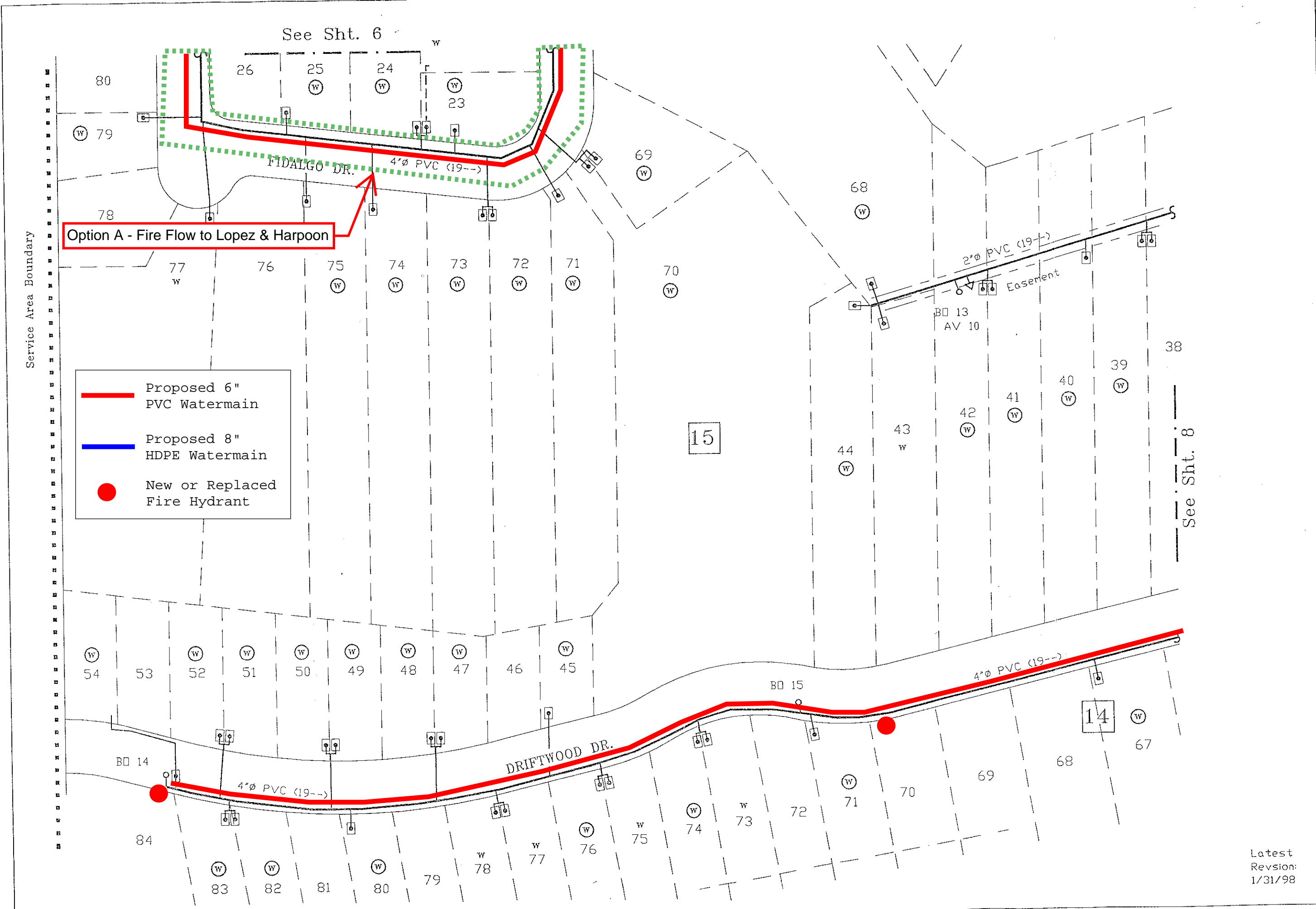
Latest Revision: 1/31/98

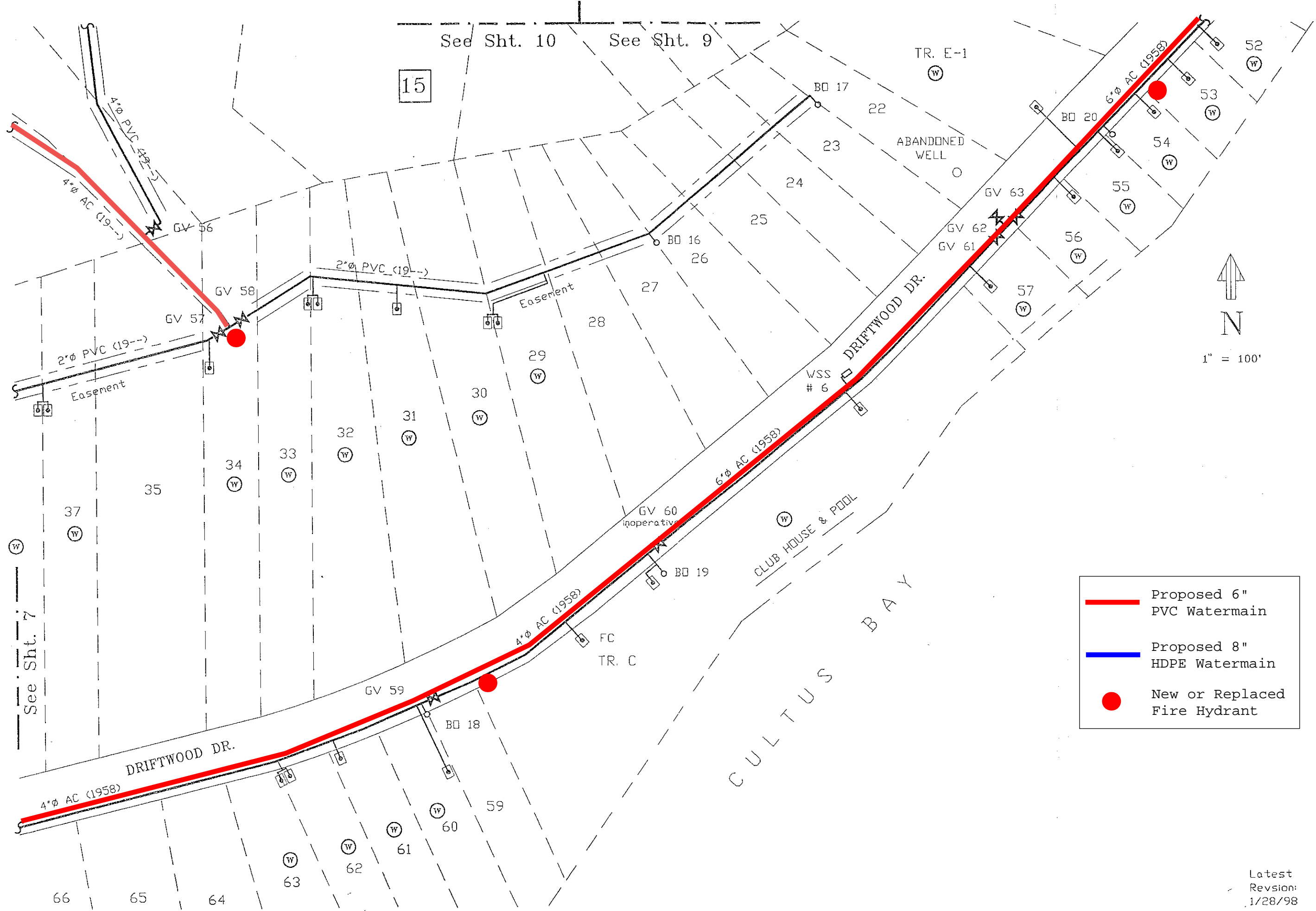
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 Coupeville, Washington 98239
 Job 297 November 1997




WATER DISTRIBUTION SYSTEM
 COMPREHENSIVE MAP

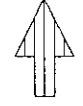
SCATCHEL HEAD WATER DISTRICT
 3792 EAST HUBBLE COURT
 Clinton, Washington 98236

Sht. 7 of 10





| | |
|---|------------------------------|
|  | Proposed 6" PVC Watermain |
|  | Proposed 8" HDPE Watermain |
|  | New or Replaced Fire Hydrant |


 N
 1" = 100'

Latest
Revision:
1/28/98

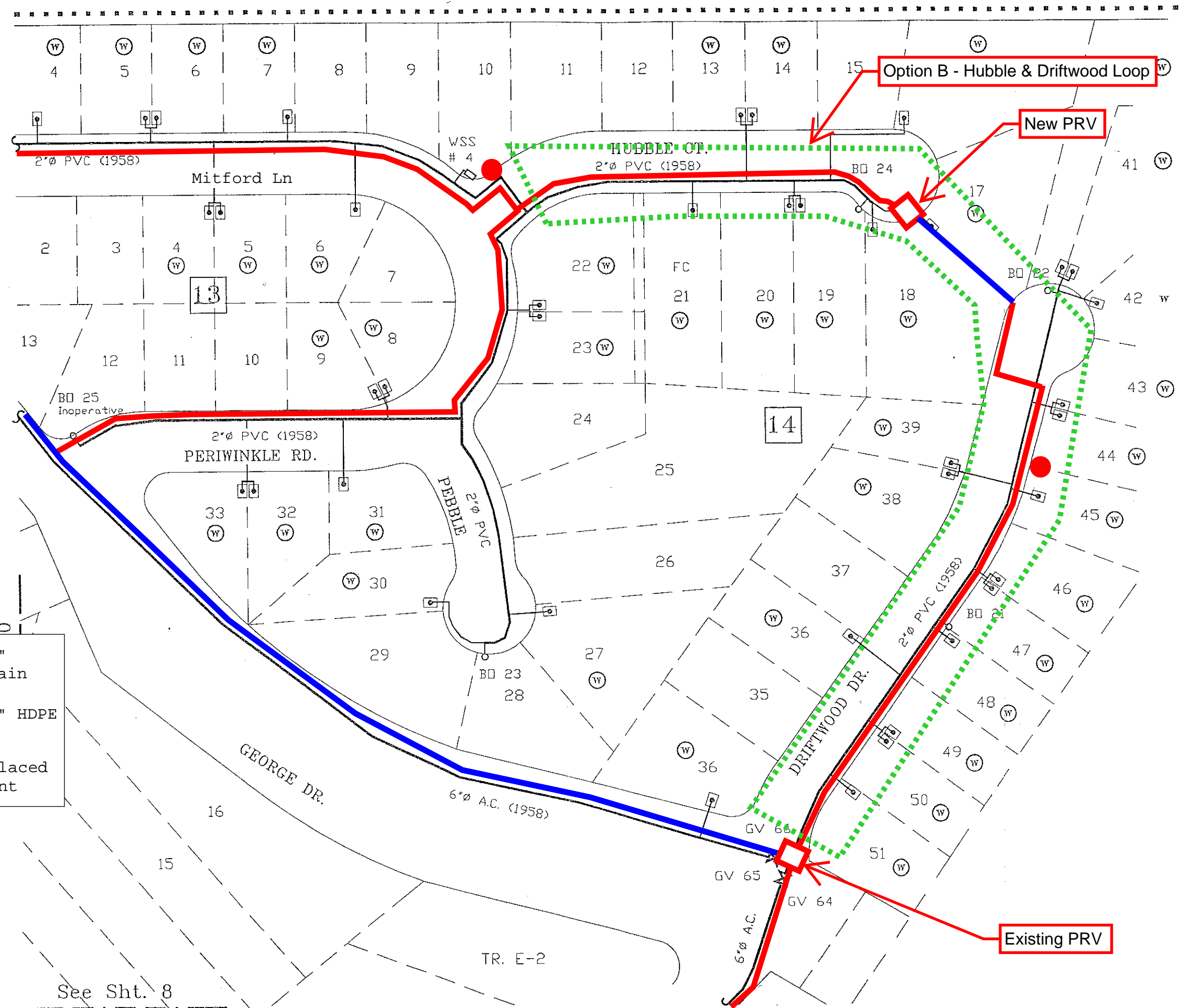
WATER DISTRIBUTION SYSTEM
 COMPREHENSIVE MAP




SCATCHET HEAD WATER DISTRICT
 3792 EAST HUBBLE COURT
 Clinton, Washington 98236

SCHAEFER & BRATTON, ENGINEERS
 P. O. Box 607
 Coupeville, Washington 98239
 Job 297 November 1997

Sht. 8 of 10

Service Area Boundary



 Proposed 6" PVC Watermain
 Proposed 6" HDPE Watermain
 New or Replaced Fire Hydrant

See Sht. 8

Latest Revision: 1/28/98

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 P. O. Box 607
 Coupeville, Washington 98239
 Job 297 November 1997

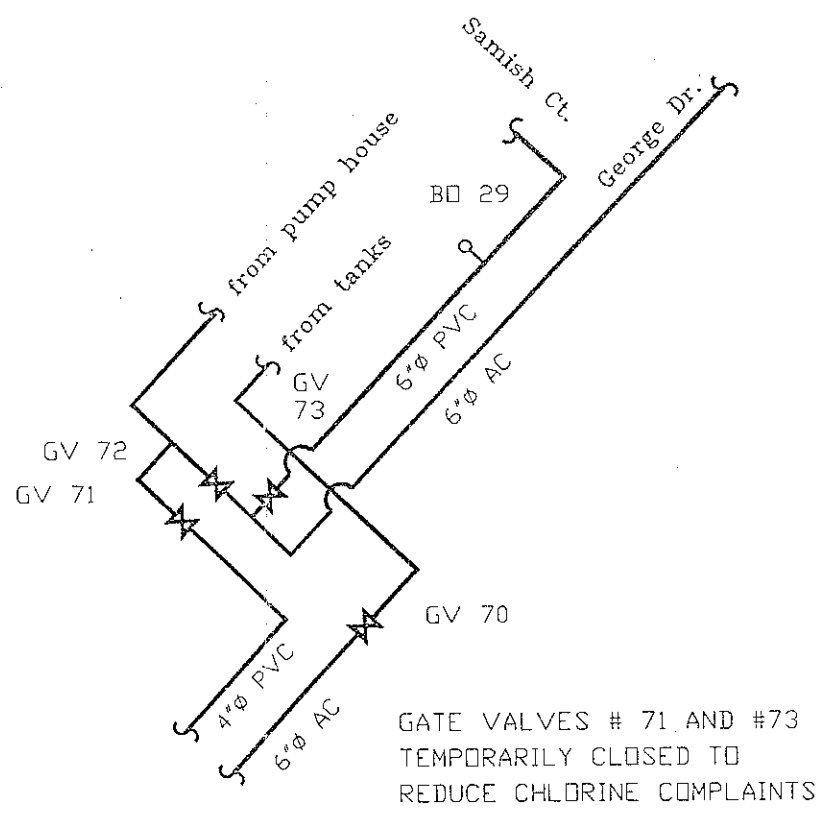
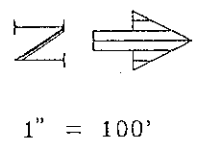
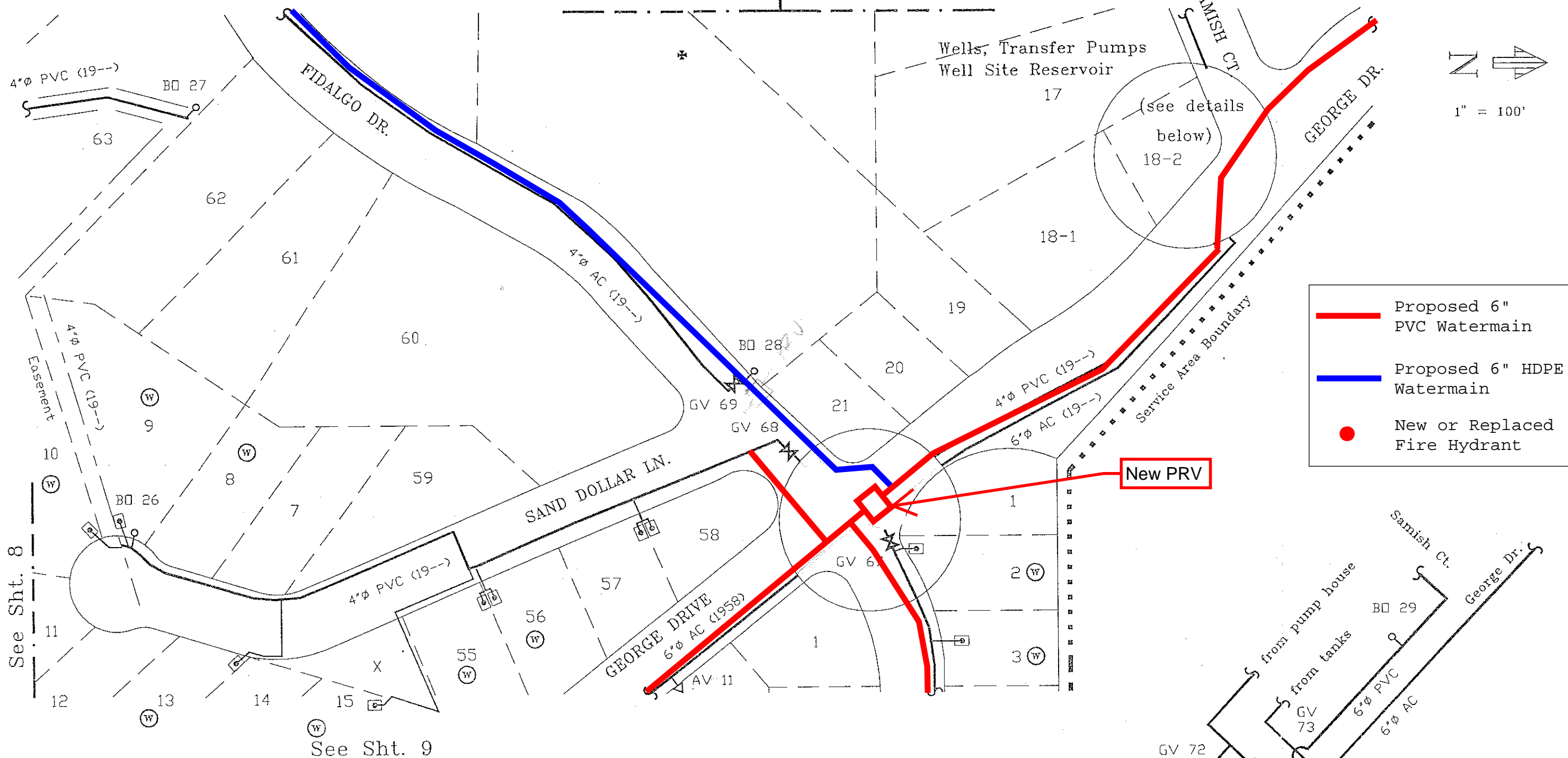
WATER DISTRIBUTION SYSTEM
 COMPREHENSIVE MAP

SCATCHET HEAD WATER DISTRICT
 3792 EAST HUBBLE COURT
 Clinton, Washington 98236

Sht. 9 of 10

See Sht. 6

See Sht. 5



George Dr. Well Site
Piping Diagram
n.t.s.

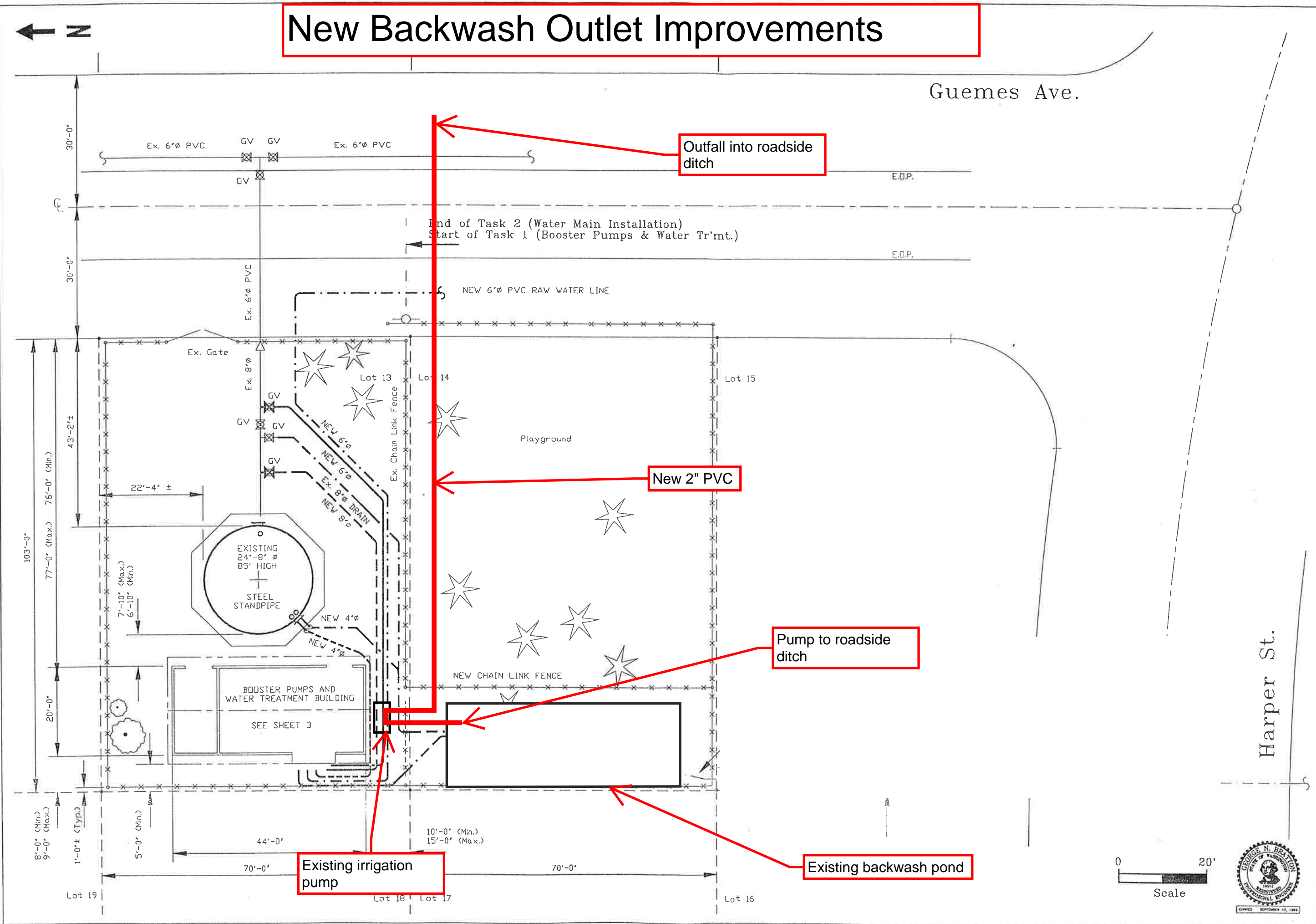
Latest Revision: 2/16/98

SCHAEFER & BRATTON, ENGINEERS
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Coupeville, Washington 98239
Job 297 November 1997

WATER DISTRIBUTION SYSTEM
COMPREHENSIVE MAP

SCATCHET HEAD WATER DISTRICT
3792 EAST HUBBLE COURT
Clinton, Washington 98236

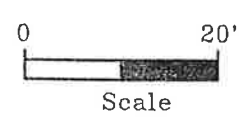
New Backwash Outlet Improvements



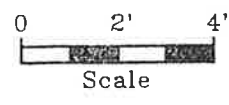
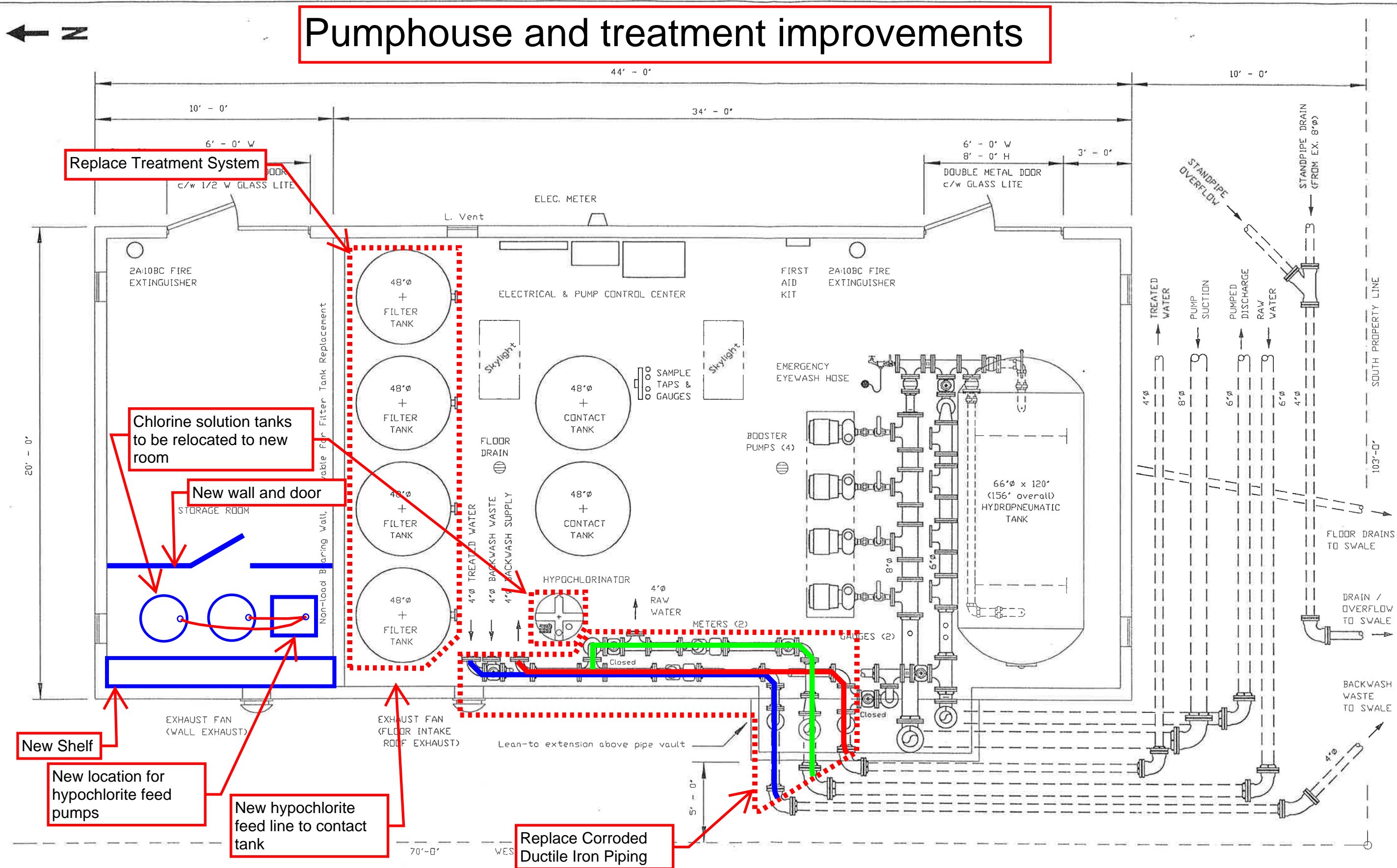
SCHAEFER & BRATTON, ENGINEERS
 P. O. Box 607
 Coupeville, Washington 98239
 Job 297 September 1998

1999 WATER SYSTEM IMPROVEMENTS
 BOOSTER PUMPS & WATER TREATMENT
 Guemes Ave. Reservoir Site Plan

SCATCHET HEAD WATER DISTRICT
 3792 EAST HUBBLE COURT
 Clinton, Washington 98236



Pumphouse and treatment improvements



12/2/98

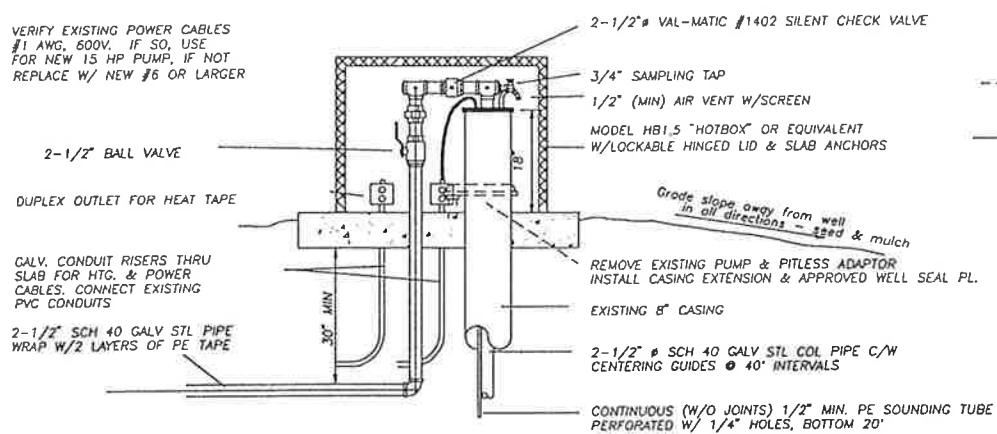
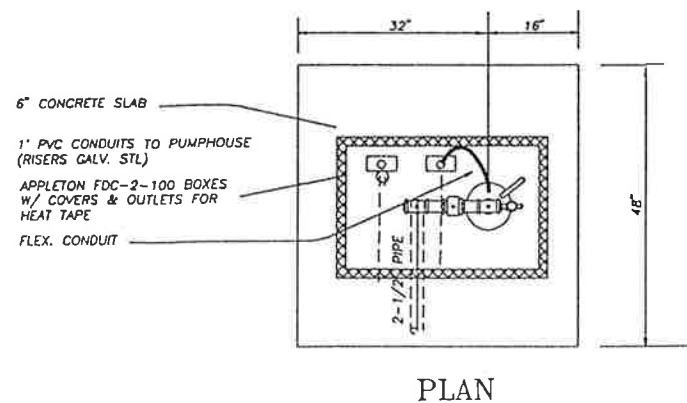


SCHAEFER & BRATTON, ENGINEERS
 P. O. Box 607
 Coupeville, Washington 98239
 Job 297 September 1998

1999 WATER SYSTEM IMPROVEMENTS
 BOOSTER PUMPS & WATER TREATMENT
 Building Layout

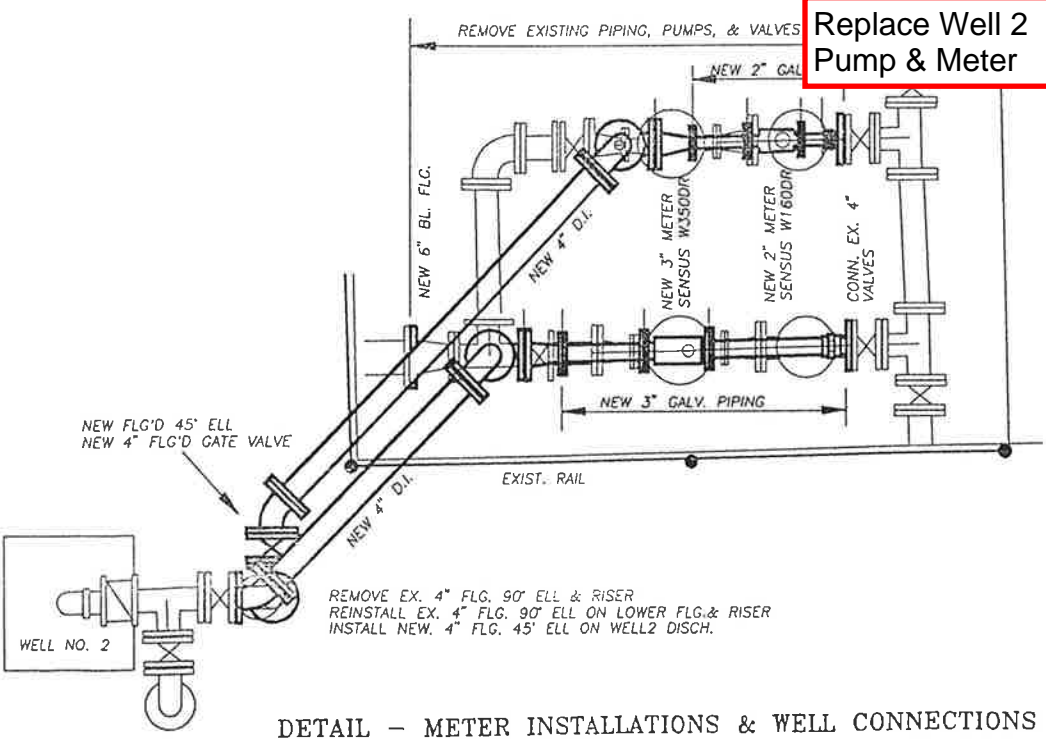
SCATCHETT HEAD WATER DISTRICT
 3792 EAST HUBBLE COURT
 Clinton, Washington 98236

Source Improvements

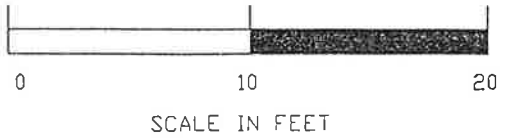
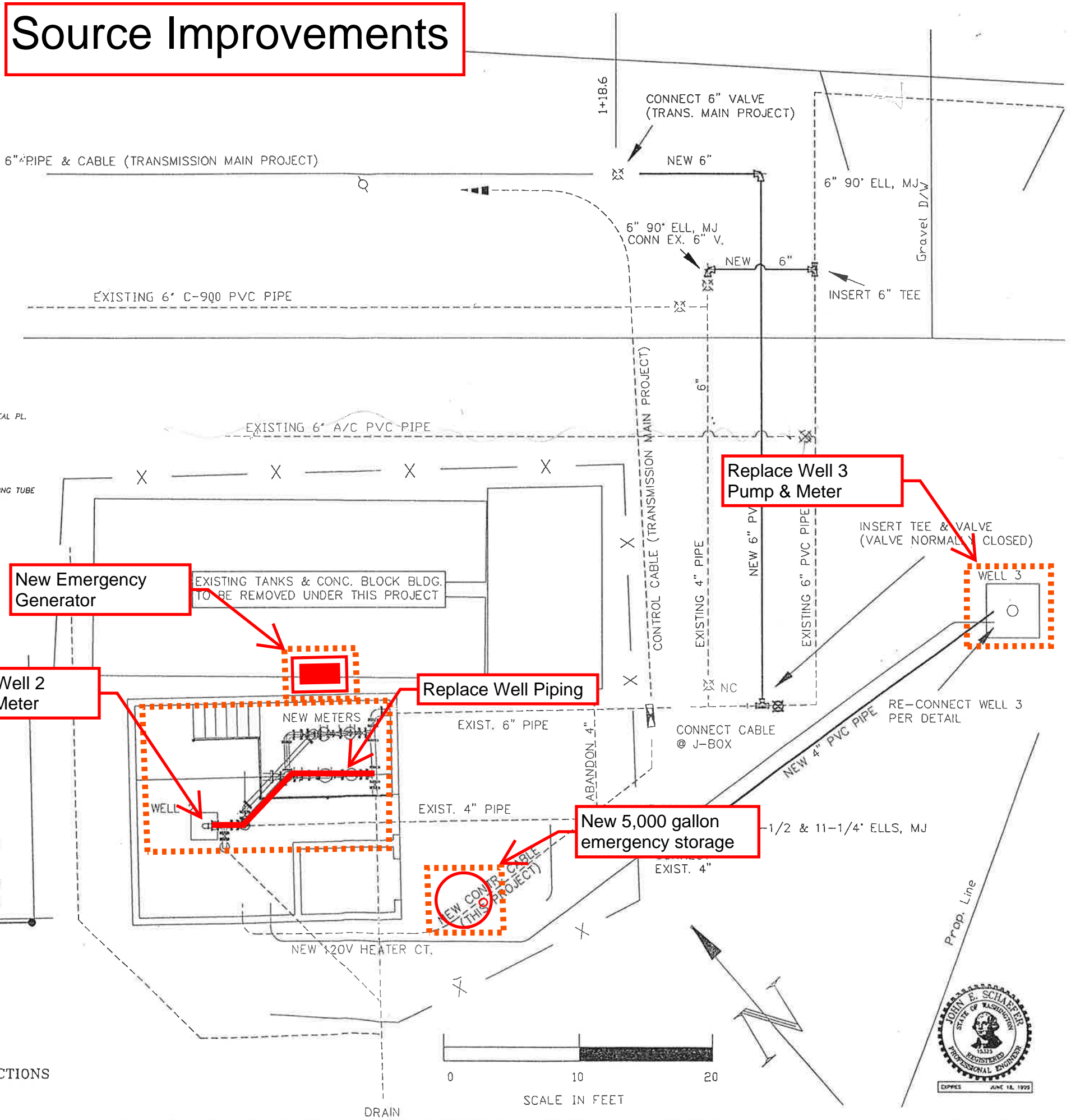


WELL NO. 3 ENCLOSURE

NOTE: EXISTING POWER CONDUIT FROM WELL 2 TERMINATES AT STARTER IN WELL 2 BLDG. EXISTING EMPTY 1\"/>



DETAIL - METER INSTALLATIONS & WELL CONNECTIONS



SCHAEFER & BRATTON, ENGINEERS
 P. O. Box 607
 Coupeville, Washington 98239
 Job 297 December 1998

1999 WATER SYSTEM IMPROVEMENTS
 EXISTING WELL AND PUMP HOUSE
 Yard Piping Modifications

SCATCHEL HEAD WATER DISTRICT
 3792 EAST HUBBLE COURT
 Clinton, Washington 98236

2/8/99

APPENDIX B Water Facility Inventory Form

WATER FACILITIES INVENTORY (WFI) FORM - Continued

| 1. SYSTEM ID NO. | 2. SYSTEM NAME | 3. COUNTY | 4. GROUP | 5. TYPE |
|------------------|------------------------------|-----------|----------|---------|
| 76470 X | SCATCHET HEAD WATER DISTRICT | ISLAND | A | Comm |

| | ACTIVE SERVICE CONNECTIONS | DOH USE ONLY! CALCULATED ACTIVE CONNECTIONS | DOH USE ONLY! APPROVED CONNECTIONS |
|---|----------------------------|--|---------------------------------------|
| 25. SINGLE FAMILY RESIDENCES (How many of the following do you have?) | | 410 | 451 |
| A. Full Time Single Family Residences (Occupied 180 days or more per year) | 410 | | |
| B. Part Time Single Family Residences (Occupied less than 180 days per year) | 0 | | |
| 26. MULTI-FAMILY RESIDENTIAL BUILDINGS (How many of the following do you have?) | | | |
| A. Apartment Buildings, condos, duplexes, barracks, dorms | 0 | | |
| B. Full Time Residential Units in the Apartments, Condos, Duplexes, Dorms that are occupied more than 180 days/year | 0 | | |
| C. Part Time Residential Units in the Apartments, Condos, Duplexes, Dorms that are occupied less than 180 days/year | 0 | | |
| 27. NON-RESIDENTIAL CONNECTIONS (How many of the following do you have?) | | | |
| A. Recreational Services and/or Transient Accommodations (Campsites, RV sites, hotel/motel/overnight units) | 0 | 0 | 0 |
| B. Institutional, Commercial/Business, School, Day Care, Industrial Services, etc. | 0 | 0 | 0 |
| 28. TOTAL SERVICE CONNECTIONS | | 410 | 451 |

| |
|---|
| 29. FULL-TIME RESIDENTIAL POPULATION |
| A. How many residents are served by this system 180 or more days per year? 900 |

| 30. PART-TIME RESIDENTIAL POPULATION | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
|---|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| A. How many part-time residents are present each month? | | | | | | | | | | | | |
| B. How many days per month are they present? | | | | | | | | | | | | |

| 31. TEMPORARY & TRANSIENT USERS | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
|--|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| A. How many total visitors, attendees, travelers, campers, patients or customers have access to the water system each month? | | | | | | | | | | | | |
| B. How many days per month is water accessible to the public? | | | | | | | | | | | | |

| 32. REGULAR NON-RESIDENTIAL USERS | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
|---|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| A. If you have schools, daycares, or businesses connected to your water system, how many students daycare children and/or employees are present each month? | | | | | | | | | | | | |
| B. How many days per month are they present? | | | | | | | | | | | | |

| 33. ROUTINE COLIFORM SCHEDULE | JAN | FEB | MAR | APR | MAY | JUN | JUL | AUG | SEP | OCT | NOV | DEC |
|-------------------------------|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|-----|
| | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 | 1 |

| 34. NITRATE SCHEDULE | QUARTERLY | ANNUALLY | ONCE EVERY 3 YEARS |
|--|-----------|----------|--------------------|
| (One Sample per source by time period) | | | |

35. Reason for Submitting WFI:

Update - Change
 Update - No Change
 Inactivate
 Re-Activate
 Name Change
 New System
 Other _____

36. I certify that the information stated on this WFI form is correct to the best of my knowledge.

SIGNATURE: _____ DATE: _____

PRINT NAME: _____ TITLE: _____

APPENDIX C Asset Inventory

Component Inventory and Assessment

| | |
|-------------------|---------------------------------------|
| System: | Scatchet Head Water District |
| PWS ID# | 76470 X |
| Location: | 7906 Guemes Ave, Clinton, WA 98236 |
| Owner: | Scatchet Head Water District |
| Operator: | King Water Management Co. |
| Operator Address: | PO Box 2243, Oak Harbor, WA 98277 |
| Prepared By: | Tabatha Dye, EIT & Robert Bennion, PE |

| Component | Component Information | Installed Date | Effective Life | Condition Rating | Critical Number | Remaining Life | Replacement Cost/Unit | Quantity | Unit | Replacement Total Cost | Inflation Rate | Replace in 6 Years? | Future Cost |
|-----------------------------|---------------------------------------|----------------|----------------|------------------|-----------------|----------------|-----------------------|----------|------|------------------------|----------------|---------------------|--------------|
| Well #2 | 10", 295' Depth | 1980 | 50 | 1 | 2 | 11 | \$ 30,000 | 1 | LS | \$ 30,000 | 2.0% | No | \$ 37,301 |
| Well #2 Pump | Goulds 160CLC030 30 HP | 1999 | 15 | 1 | 2 | -5 | \$ 6,000 | 1 | LS | \$ 6,000 | 2.0% | Yes | \$ 6,000 |
| Well #3 | 8", 403' Depth | 1997 | 50 | 1 | 2 | 28 | \$ 30,000 | 1 | LS | \$ 30,000 | 2.0% | No | \$ 52,231 |
| Well #3 Pump | Goulds 70J15 15 HP | 1999 | 15 | 1 | 2 | -5 | \$ 6,000 | 1 | LS | \$ 6,000 | 2.0% | Yes | \$ 6,000 |
| Well Meters | | 1995 | 25 | 2 | 2 | 1 | \$ 1,500 | 2 | EA | \$ 3,000 | 2.0% | Yes | \$ 3,060 |
| Well Controls | | 1995 | 15 | 2 | 1 | -9 | \$ 2,000 | 1 | LS | \$ 2,000 | 2.0% | Yes | \$ 2,000 |
| Chlorinator | LMI Series A17 | 2001 | 30 | 2 | 2 | 12 | \$ 2,000 | 1 | LS | \$ 2,000 | 2.0% | No | \$ 2,536 |
| Treatment System | Filtration: (4) 48"D, 463 gal Tanks | 2001 | 30 | 3 | 1 | 12 | \$ 20,000 | 1 | LS | \$ 20,000 | 2.0% | No | \$ 25,365 |
| Storage Reservoir #1 | Guemes 300,000 (24.5' D x 85' T) | 1980 | 60 | 3 | 1 | 21 | \$ 2 | 300,000 | GAL | \$ 450,000 | 2.0% | No | \$ 682,050 |
| Storage Reservoir #2 | Maple Point 120,000 (14.6' D x 95' T) | 1997 | 60 | 3 | 2 | 38 | \$ 2 | 120,000 | GAL | \$ 180,000 | 2.0% | No | \$ 382,014 |
| Reservoir Controls | | 1999 | 15 | 4 | 2 | -5 | \$ 5,000 | 1 | LS | \$ 5,000 | 2.0% | Yes | \$ 5,000 |
| Pressure Tank | Canal Boiler Works (66" D x 10' L) | 1980 | 10 | 2 | 1 | -29 | \$ 10 | 2,120 | GAL | \$ 21,200 | 2.0% | Yes | \$ 21,200 |
| Air Charger | Whitewater Air Rite D610 | 1999 | 15 | 2 | 2 | -5 | \$ 3,000 | 1 | EA | \$ 3,000 | 2.0% | Yes | \$ 3,000 |
| Booster Pump #1-4 | Aurora Series 340/360 7.5 HP | 1999 | 15 | 4 | 2 | -5 | \$ 3,000 | 4 | EA | \$ 12,000 | 2.0% | Yes | \$ 12,000 |
| Booster Pump Controls | | 1999 | 15 | 3 | 2 | -5 | \$ 10,000 | 1 | LS | \$ 10,000 | 2.0% | Yes | \$ 10,000 |
| Distribution System Piping* | 8" PVC | 1997 | 50 | 2 | 5 | 28 | \$ 160 | 567 | LF | \$ 90,720 | 2.0% | No | \$ 157,946 |
| Distribution System Piping* | 6 & 8" DI | 1958 | 50 | 3 | 5 | -11 | \$ 200 | 1,252 | LF | \$ 250,400 | 2.0% | Yes | \$ 250,400 |
| Distribution System Piping* | 6" PVC | 1996 | 50 | 3 | 2 | 27 | \$ 150 | 9,212 | LF | \$ 1,381,800 | 2.0% | No | \$ 2,358,576 |
| Distribution System Piping* | 6" AC | 1958 | 50 | 3 | 5 | -11 | \$ 200 | 9,755 | LF | \$ 1,951,000 | 2.0% | Yes | \$ 1,951,000 |
| Distribution System Piping* | 4" PVC | 1997 | 50 | 2 | 2 | 28 | \$ 120 | 8,695 | LF | \$ 1,043,400 | 2.0% | No | \$ 1,816,585 |
| Distribution System Piping* | 2/2.5 other | 1958 | 50 | 2 | 5 | -11 | \$ 100 | 6,636 | LF | \$ 663,600 | 2.0% | Yes | \$ 663,600 |
| Dedicated Fill Line Piping | 6" PVC | 1997 | 50 | 1 | 1 | 28 | \$ 150 | 3,135 | LF | \$ 470,250 | 2.0% | No | \$ 818,717 |

| | | | | | | | | | | | | | |
|----------------------------------|------------------------------|------|----|--------|-------|-----|-----------|-------|------|------------|------|-----|------------|
| Hydrants* | | 1980 | 50 | 3 | 4 / 5 | 11 | \$ 5,000 | 20 | EA | \$ 100,000 | 2.0% | No | \$ 124,337 |
| Gate Valves* | | 1980 | 20 | 2 | 4 / 5 | -19 | \$ 2,500 | 70 | EA | \$ 175,000 | 2.0% | Yes | \$ 175,000 |
| Air-release Valves* | | 1980 | 20 | 2 | 4 / 5 | -19 | \$ 3,000 | 18 | EA | \$ 54,000 | 2.0% | Yes | \$ 54,000 |
| Blow-offs* | | 1980 | 20 | 2 | 4 / 5 | -19 | \$ 3,000 | 14 | EA | \$ 42,000 | 2.0% | Yes | \$ 42,000 |
| Pressure Reducing Valve Stations | Fidalgo PRV Station: | 1980 | 20 | 3 | 2 | -19 | \$ 40,000 | 1 | EA | \$ 40,000 | 2.0% | Yes | \$ 40,000 |
| | Fidalgo/George PRV Station: | 1980 | 20 | 3 | 2 | -19 | \$ 40,000 | 1 | EA | \$ 40,000 | 2.0% | Yes | \$ 40,000 |
| | Driftwood Drive PRV Station: | 2007 | 20 | 1 | 2 | 8 | \$ 40,000 | 1 | EA | \$ 40,000 | 2.0% | No | \$ 46,866 |
| Service meters | | 1980 | 15 | Varies | 4 / 5 | -24 | \$ 200 | 410 | EA | \$ 82,000 | 2.0% | Yes | \$ 82,000 |
| Generator | | 1980 | 50 | 2 | 3 | 11 | \$ 6,000 | | EA | \$ - | 2.0% | No | \$ - |
| Propane Tank | | 1980 | 30 | 2 | 3 | -9 | \$ 2,000 | | EA | \$ - | 2.0% | Yes | \$0 |
| Pumphouse | | 1980 | 75 | 3 | 3 | 36 | \$ 200 | 1,125 | SF | \$ 225,000 | 2.0% | No | \$ 458,975 |
| Facility Maintenance | | 1980 | 50 | n/a | | 11 | \$ 2,000 | 6 | Year | \$ 12,000 | | No | \$ 12,000 |

*From 1998 WSP

Major Anticipated Projects

- Treatment System Replacement
- Old Water Main Replacement
- 2nd Line to Beach
- Looping Periwinkle to George
- Expansion West

Total Cost Estimate for 6-year \$10,329,758

APPENDIX D Financial Information

System Financial Information

| | 2015 | 2016 | 2017 | 2018 |
|-----------------------------------|------------|------------|------------|------------|
| REVENUES | | | | |
| Water Fees | 134,396.46 | 132,192.15 | 137,928.41 | 134,670.49 |
| Late Fees | 773.47 | 420.63 | 785.14 | 402.09 |
| Reimbursed Expenses | 3,382.00 | 2,297.35 | 2,728.00 | 2,261.00 |
| Total Income | 138,551.93 | 134,910.13 | 141,441.55 | 137,333.58 |
| EXPENSES | | | | |
| Bond | | | | |
| Transfer to Bond Fund | 45,000.00 | 45,000.00 | 45,000.00 | 45,000.00 |
| Direct Salaries and Wages | | | | |
| Manager Salary | 7,200.00 | 7,200.00 | 7,200.00 | 7,200.00 |
| Commissioners Pay | 3,648.00 | 3,762.00 | 3,534.00 | 4,186.00 |
| Meter Reading | 600.00 | 600.00 | 600.00 | 700.00 |
| Payroll Expenses | 1,140.56 | 1,147.80 | 1,156.44 | 1,136.09 |
| Total Direct Salaries and Wages | 12,588.56 | 12,709.80 | 12,490.44 | 13,222.09 |
| Water Maintenance | | | | |
| Water Management | 12,348.00 | 12,348.00 | 12,348.00 | 13,058.00 |
| Water Repairs and Maintenance | 7,385.06 | 9,402.05 | 7,356.54 | 17,512.05 |
| Water Testing | 1,455.50 | 1,548.00 | 1,523.00 | 3,071.00 |
| Chlorine and Chemicals | 2,518.53 | 2,325.60 | 2,706.46 | 2,923.83 |
| Reservoir Cleaning | 0.00 | 3,206.65 | 0.00 | 0.00 |
| Sanitary Survey | 1,142.92 | 0.00 | 0.00 | 0.00 |
| Capital Improvement | 2,450.10 | 0.00 | 0.00 | 0.00 |
| Supplies/Parts | 0.00 | 0.00 | 59.17 | 262.51 |
| Flushing | 0.00 | 0.00 | 0.00 | 1,747.90 |
| Water System Site Maintenance | 0.00 | 0.00 | 0.00 | 19.90 |
| Total Water Maintenance | 27,300.11 | 28,830.30 | 23,993.17 | 38,595.19 |
| Utilities | | | | |
| Telephone | 214.44 | 214.44 | 214.44 | 214.44 |
| Propane | 441.79 | 189.59 | 92.40 | 92.51 |
| Electric | 8,886.43 | 11,319.06 | 11,145.02 | 13,566.50 |
| Total Utilities | 9,542.66 | 11,723.09 | 11,451.86 | 13,873.45 |
| General and Administrative | | | | |
| Liability Insurance | 4,397.00 | 4,503.00 | 4,657.00 | 5,017.00 |
| Dues and Subscriptions | 637.23 | 651.99 | 422.70 | 629.05 |
| Island County NSF Fee | 40.00 | 80.00 | 240.00 | 160.00 |
| Licenses and Permits | 724.00 | 724.00 | 724.00 | 1,202.76 |
| Office Supplies | 248.64 | 153.30 | 294.66 | 85.76 |
| Billing Cards and Stamps | 1,329.68 | 1,083.30 | 1,451.09 | 1,545.26 |
| Certified Letter Fees | 2,241.59 | 2,233.79 | 2,299.03 | 1,630.50 |
| Mailings | 0.00 | 0.00 | 0.00 | 1,946.05 |

| | | | | |
|----------------------------------|------------|------------|------------|------------|
| Lien Filling Fees | 507.00 | 154.44 | 155.44 | 190.23 |
| Printing and Reproduction | 44.46 | 75.60 | 234.55 | 70.51 |
| Professional Development | 0.00 | 152.89 | 270.40 | 0.00 |
| Freedom of Information Response | 0.00 | 0.00 | 0.00 | 1,395.71 |
| Total General and Administrative | 10,169.60 | 9,812.31 | 10,748.87 | 12,477.12 |
| Professional Services | | | | |
| Engineering | 0.00 | 600.00 | 13,780.49 | 6,345.49 |
| Accounting | 9,600.00 | 9,600.00 | 9,600.00 | 10,080.00 |
| Audit | 0.00 | 1,391.12 | 205.44 | 145.66 |
| Legal Fees | 0.00 | 0.00 | 0.00 | 1,890.50 |
| Subcontractor/Maintenance | 0.00 | 0.00 | 2,282.70 | 0.00 |
| Total Professional Services | 9,600.00 | 11,591.12 | 25,868.63 | 18,461.65 |
| Taxes | | | | |
| State Utility Tax | -150.55 | 8,136.59 | 6,943.22 | 7,240.78 |
| Property | 78.26 | 78.26 | 78.26 | 78.26 |
| Total Taxes | -72.29 | 8,214.85 | 7,021.48 | 7,319.04 |
| Total Expenses | 114,128.64 | 127,881.47 | 136,574.45 | 150,344.25 |
| NET | | | | |
| Total Income | 138,551.93 | 134,910.13 | 141,441.55 | 137,333.58 |
| Total Expenses | 114,128.64 | 127,881.47 | 136,574.45 | 150,344.25 |
| Net Income | 24,423.29 | 7,028.66 | 4,867.10 | -13,010.67 |

| | Year 1 2020 | Year 2 2021 | Year 3 2022 | Year 4 2023 | Year 5 2024 | Year 6 2025 |
|----------------------------------|---|----------------|----------------|----------------|----------------|----------------|
| REVENUES | | | | | | |
| Water Fees | \$168,000.00 | \$201,600.00 | \$236,300.00 | \$254,100.00 | \$254,100.00 | \$254,100.00 |
| Late Fees | \$400.00 | \$400.00 | \$400.00 | \$400.00 | \$400.00 | \$400.00 |
| Reimbursed Expenses | \$2,500.00 | \$2,500.00 | \$2,500.00 | \$2,500.00 | \$2,500.00 | \$2,500.00 |
| Total Income | \$170,900.00 | \$204,500.00 | \$239,200.00 | \$257,000.00 | \$257,000.00 | \$257,000.00 |
| EXPENSES | | | | | | |
| Direct Salaries and Wages | | | | | | |
| Manager Salary | \$7,200.00 | \$7,200.00 | \$7,700.00 | \$7,700.00 | \$8,200.00 | \$8,200.00 |
| Commissioners Pay | \$4,000.00 | \$4,400.00 | \$4,600.00 | \$4,600.00 | \$4,600.00 | \$4,800.00 |
| Meter Reading | \$700.00 | \$900.00 | \$900.00 | \$900.00 | \$900.00 | \$900.00 |
| Payroll Expenses | \$1,150.00 | \$1,350.00 | \$1,350.00 | \$1,550.00 | \$1,550.00 | \$1,550.00 |
| Total Direct Salaries and Wages | \$13,050.00 | \$13,850.00 | \$14,550.00 | \$14,750.00 | \$15,250.00 | \$15,450.00 |
| Water Maintenance | | | | | | |
| Water Management | \$13,100.00 | \$14,000.00 | \$14,000.00 | \$15,000.00 | \$15,000.00 | \$15,000.00 |
| Water Repairs and Maintenance | \$10,500.00 | \$10,500.00 | \$10,500.00 | \$10,500.00 | \$10,500.00 | \$10,500.00 |
| Water Testing | \$2,750.00 | \$2,750.00 | \$2,750.00 | \$3,000.00 | \$3,000.00 | \$3,250.00 |
| Chlorine and Chemicals | \$3,600.00 | \$3,600.00 | \$3,600.00 | \$3,800.00 | \$3,800.00 | \$3,800.00 |
| Reservoir Cleaning | \$0.00 | \$0.00 | \$4,500.00 | \$0.00 | \$0.00 | \$0.00 |
| Sanitary Survey | \$2,000.00 | \$0.00 | \$0.00 | \$3,000.00 | \$0.00 | \$0.00 |
| Capital Improvement | See Capital Improvements Budget in Appendix O | | | | | |
| Supplies/Parts | \$300.00 | \$300.00 | \$400.00 | \$400.00 | \$500.00 | \$500.00 |
| Flushing | \$2,000.00 | \$2,000.00 | \$2,000.00 | \$3,000.00 | \$3,000.00 | \$3,000.00 |
| Total Water Maintenance | \$34,250.00 | \$33,150.00 | \$37,750.00 | \$38,700.00 | \$35,800.00 | \$36,050.00 |

| Utilities | | | | | | |
|----------------------------------|-------------|-------------|-------------|-------------|-------------|-------------|
| Telephone | \$250.00 | \$250.00 | \$250.00 | \$250.00 | \$300.00 | \$300.00 |
| Propane | \$150.00 | \$150.00 | \$150.00 | \$150.00 | \$150.00 | \$150.00 |
| Electric | \$14,000.00 | \$14,150.00 | \$14,600.00 | \$14,600.00 | \$14,600.00 | \$14,900.00 |
| Total Utilities | \$14,400.00 | \$14,550.00 | \$15,000.00 | \$15,000.00 | \$15,050.00 | \$15,350.00 |
| General and Administrative | | | | | | |
| Liability Insurance | \$5,100.00 | \$5,100.00 | \$5,500.00 | \$5,500.00 | \$6,000.00 | \$6,000.00 |
| Dues and Subscriptions | \$650.00 | \$650.00 | \$650.00 | \$700.00 | \$700.00 | \$800.00 |
| Island County NSF Fee | \$200.00 | \$200.00 | \$200.00 | \$250.00 | \$250.00 | \$250.00 |
| Licenses and Permits | \$1,250.00 | \$1,250.00 | \$1,250.00 | \$1,250.00 | \$1,250.00 | \$1,250.00 |
| Office Supplies | \$250.00 | \$250.00 | \$250.00 | \$250.00 | \$250.00 | \$250.00 |
| Billing Cards and Stamps | \$1,600.00 | \$1,600.00 | \$1,600.00 | \$1,600.00 | \$1,600.00 | \$1,600.00 |
| Certified Letter Fees | \$3,000.00 | \$3,000.00 | \$3,500.00 | \$3,500.00 | \$3,500.00 | \$4,000.00 |
| Mailings | \$1,500.00 | \$1,500.00 | \$1,500.00 | \$2,000.00 | \$2,000.00 | \$2,000.00 |
| Lien Filing Fees | \$200.00 | \$200.00 | \$200.00 | \$200.00 | \$200.00 | \$200.00 |
| Printing and Reproduction | \$100.00 | \$100.00 | \$100.00 | \$100.00 | \$100.00 | \$100.00 |
| Professional Development | \$500.00 | \$500.00 | \$500.00 | \$500.00 | \$500.00 | \$500.00 |
| Freedom of Information Response | \$1,500.00 | \$1,500.00 | \$1,500.00 | \$1,500.00 | \$1,500.00 | \$1,500.00 |
| Total General and Administrative | \$15,850.00 | \$15,850.00 | \$16,750.00 | \$17,350.00 | \$17,850.00 | \$18,450.00 |
| Professional Services | | | | | | |
| Engineering | \$15,000.00 | \$15,000.00 | \$18,000.00 | \$18,000.00 | \$20,000.00 | \$20,000.00 |
| Accounting | \$11,000.00 | \$12,000.00 | \$12,000.00 | \$13,000.00 | \$14,000.00 | \$14,000.00 |
| Audit | \$1,000.00 | \$1,000.00 | \$2,000.00 | \$2,000.00 | \$2,500.00 | \$2,500.00 |
| Legal Fees | \$2,000.00 | \$2,000.00 | \$2,000.00 | \$3,000.00 | \$3,000.00 | \$3,000.00 |
| Subcontractor/Maintenance | \$2,500.00 | \$2,500.00 | \$2,500.00 | \$3,000.00 | \$3,000.00 | \$3,000.00 |
| Total Professional Services | \$31,500.00 | \$32,500.00 | \$36,500.00 | \$39,000.00 | \$42,500.00 | \$42,500.00 |
| Taxes | | | | | | |

| | | | | | | |
|-------------------|--------------|--------------|--------------|--------------|--------------|--------------|
| State Utility Tax | \$8,000.00 | \$9,600.00 | \$11,300.00 | \$12,100.00 | \$12,100.00 | \$12,100.00 |
| Property | \$100.00 | \$100.00 | \$100.00 | \$100.00 | \$100.00 | \$100.00 |
| Total Taxes | \$8,100.00 | \$9,700.00 | \$11,400.00 | \$12,200.00 | \$12,200.00 | \$12,200.00 |
| | | | | | | |
| Total Expenses | \$117,150.00 | \$119,600.00 | \$131,950.00 | \$137,000.00 | \$138,650.00 | \$140,000.00 |
| | | | | | | |
| NET | | | | | | |
| Total Income | \$170,900.00 | \$204,500.00 | \$239,200.00 | \$257,000.00 | \$257,000.00 | \$257,000.00 |
| Total Expenses | \$117,150.00 | \$119,600.00 | \$131,950.00 | \$137,000.00 | \$138,650.00 | \$140,000.00 |
| Net Income | \$53,750.00 | \$84,900.00 | \$107,250.00 | \$120,000.00 | \$118,350.00 | \$117,000.00 |

Full Project Cost Estimate

ENGINEER'S PRELIMINARY CONSTRUCTION COST ESTIMATE

CLIENT: Scatchet Head Water District
PROJECT: Full System Improvement Project
DATE: October 2020

| NO. | ITEM | UNIT | UNIT COST | QUANTITY | TOTAL COST |
|--|---|------|---------------|----------|------------|
| Distribution System Improvements | | | | | |
| 1 | Mobilization | LS | \$ 102,000.00 | 1 | \$102,000 |
| 2 | Project Temporary Traffic Control | LS | \$ 10,000.00 | 1 | \$10,000 |
| 3 | Connection to existing waterline | EA | \$ 3,500.00 | 11 | \$38,500 |
| 4 | 6" PVC C-900 Water Main (Blakely Ave) | LF | \$ 65.00 | 1,735 | \$112,775 |
| 5 | 6" PVC C-900 Water Main (Pear St) | LF | \$ 65.00 | 215 | \$13,975 |
| 6 | 6" PVC C-900 Water Main (Hat St) | LF | \$ 65.00 | 310 | \$20,150 |
| 7 | 6" PVC C-900 Water Main (San Juan Ave) | LF | \$ 65.00 | 230 | \$14,950 |
| 8 | 6" PVC C-900 Water Main (Casey St) | LF | \$ 65.00 | 340 | \$22,100 |
| 9 | 6" PVC C-900 Water Main (Guemes Ave) | LF | \$ 65.00 | 730 | \$47,450 |
| 10 | 6" PVC C-900 Water Main (Harper St) | LF | \$ 65.00 | 530 | \$34,450 |
| 11 | 6" PVC C-900 Water Main (George Dr) | LF | \$ 65.00 | 3,720 | \$241,800 |
| 12 | 6" PVC C-900 Water Main (Mitford Ln) | LF | \$ 65.00 | 710 | \$46,150 |
| 13 | 6" PVC C-900 Water Main (Pebble & Periwinkle) | LF | \$ 65.00 | 640 | \$41,600 |
| 14 | 6" PVC C-900 Water Main (Harpoon Ln) | LF | \$ 65.00 | 670 | \$43,550 |
| 15 | 6" PVC C-900 Water Main (Driftwood) | LF | \$ 65.00 | 2,850 | \$185,250 |
| 16 | 12" Road Bore & Casing Pipe | LF | \$ 300.00 | 320 | \$96,000 |
| 17 | PRV Station (Mitford & Harpoon) | LS | \$ 40,000.00 | 2 | \$80,000 |
| 19 | Water Service | EA | \$ 1,500.00 | 173 | \$259,500 |
| 20 | Sample Stations | EA | \$ 5,000.00 | 4 | \$20,000 |
| 21 | Fire Hydrants | EA | \$ 5,000.00 | 8 | \$40,000 |
| Pumphouse & Treatment Improvements | | | | | |
| 22 | New Treatment Filter System | LS | \$ 75,000.00 | 1 | \$75,000 |
| 23 | New Wall, Door and Shelf (for chemicals) | LS | \$ 4,500.00 | 1 | \$4,500 |
| 24 | Hypochlorite Feed Line Reconnection | LS | \$ 1,500.00 | 1 | \$1,500 |
| 25 | 4" Ductile Iron Piping | LF | \$ 100.00 | 50 | \$5,000 |
| 26 | 4" Meter | EA | \$ 3,000.00 | 2 | \$6,000 |
| 27 | 4" Gate Valve | EA | \$ 2,500.00 | 5 | \$12,500 |
| Source Improvements | | | | | |
| 28 | New Submersible Well Pumps | EA | \$ 10,000.00 | 2 | \$20,000 |
| 29 | Well Meters | EA | \$ 1,500.00 | 2 | \$3,000 |
| 30 | 25 kW Generator and Concrete Pad | LS | \$ 15,000.00 | 1 | \$15,000 |
| 31 | Propane Tank | EA | \$ 2,000.00 | 1 | \$2,000 |
| 32 | 5,000 Gallon Storage Tank | EA | \$ 10,000.00 | 1 | \$10,000 |
| 33 | 3" DI Well Piping | LF | \$ 90.00 | 15 | \$1,350 |
| Optional A - Fire Flow to Lopez & Harpoon | | | | | |
| 34 | 6" PVC C-900 Water Main (Orcas Dr) | LF | \$ 65.00 | 505 | \$32,825 |
| 35 | 6" PVC C-900 Water Main (Lopez Dr) | LF | \$ 65.00 | 290 | \$18,850 |
| 36 | 8" HDPE Water Main (Fidalgo Dr) | LF | \$ 85.00 | 915 | \$77,775 |
| 37 | 12" Road Bore & Casing Pipe | LF | \$ 300.00 | 100 | \$30,000 |
| 38 | Fire Hydrants | EA | \$ 5,000.00 | 2 | \$10,000 |
| Option B - Hubble to Driftwood Loop | | | | | |
| 39 | 6" PVC C-900 Water Main (Lopez Dr) | LF | \$ 65.00 | 370 | \$24,050 |
| 40 | 6" PVC C-900 Water Main (Driftwood Dr) | LF | \$ 65.00 | 625 | \$40,625 |
| 41 | PRV Station (Mitford & Harpoon) | LS | \$ 40,000.00 | 1 | \$40,000 |
| 42 | Directional Drill Installation - 6" HDPE Water Main | LF | \$ 300.00 | 200 | \$60,000 |
| Option C - Fidalgo Loop | | | | | |
| 43 | 6" HDPE Water Main - Pipe Bursting (Fidalgo Dr) | | \$ 150.00 | 1,210 | \$181,500 |

| | |
|---|--------------------|
| Construction Cost = | \$2,141,675 |
| Contingency (20%) = | \$428,335 |
| Sales Tax (8.7%) = | \$224,000 |
| Total Estimated Construction Cost = | \$2,794,000 |
| Permitting Fees, Engineering, Survey, etc. (15%) | \$279,000 |
| Rough Estimate of Project Total | \$3,070,000 |

Alternates Cost Analysis

ENGINEER'S PRELIMINARY CONSTRUCTION COST ESTIMATE

CLIENT: Scatchet Head Water District

PROJECT: Distribution System Options

DATE: October 2020

| Option 1: Replace Aging Watermains | | | | | |
|---|---|------|--------------|---|--------------------|
| NO. | ITEM | UNIT | UNIT COST | PROJECT TOTAL | |
| | | | | QUANTITY | TOTAL COST |
| 1 | Mobilization | LS | \$ 89,000.00 | 1 | \$89,000 |
| 2 | Project Temporary Traffic Control | LS | \$ 10,000.00 | 1 | \$10,000 |
| 3 | Connection to existing waterline | EA | \$ 3,500.00 | 11 | \$38,500 |
| 4 | PVC Pipe for Water Main, 6 in. Diameter | LF | \$ 65.00 | 15,680 | \$1,019,200 |
| 5 | HDPE Pipe for Water Main, 8 in. Diameter | LF | \$ 85.00 | 915 | \$77,775 |
| 6 | PRV Stations | LS | \$ 40,000.00 | 3 | \$120,000 |
| 7 | Directional Drill - Road Bores and Slope Installation | LF | \$ 300.00 | 620 | \$186,000 |
| 8 | Water Service | EA | \$ 1,500.00 | 173 | \$259,500 |
| 9 | Sample Stations | EA | \$ 5,000.00 | 4 | \$20,000 |
| 10 | Fire Hydrants | EA | \$ 5,000.00 | 10 | \$50,000 |
| | | | | Construction Cost = | \$1,870,000 |
| | | | | Contingency (20%) = | \$374,000 |
| | | | | Sales Tax (8.7%) = | \$195,000 |
| | | | | Total Estimated Construction Cost = | \$2,439,000 |
| | | | | Permitting Fees, Engineering, Survey, etc. (15%) | \$366,000 |
| | | | | Rough Estimate of Project Total | \$2,810,000 |

| Option 2: Pipe Bursting | | | | | |
|--------------------------------|---|------|---------------|---|--------------------|
| NO. | ITEM | UNIT | UNIT COST | PROJECT TOTAL | |
| | | | | QUANTITY | TOTAL COST |
| 1 | Mobilization | LS | \$ 165,700.00 | 1 | \$165,700 |
| 2 | Project Temporary Traffic Control | LS | \$ 10,000.00 | 1 | \$10,000 |
| 3 | Connection to existing waterline | EA | \$ 3,500.00 | 11 | \$38,500 |
| 4 | Pipe Bursting | LF | \$ 160.00 | 16,595 | \$2,655,200 |
| 5 | Temporary Water Service | LS | \$ 100,000.00 | 1 | \$100,000 |
| 6 | PRV Stations | LS | \$ 40,000.00 | 3 | \$120,000 |
| 7 | Directional Drill - Road Bores and Slope Installation | LF | \$ 300.00 | 200 | \$60,000 |
| 8 | Water Service | EA | \$ 1,500.00 | 173 | \$259,500 |
| 9 | Sample Stations | EA | \$ 5,000.00 | 4 | \$20,000 |
| 10 | Fire Hydrants | EA | \$ 5,000.00 | 10 | \$50,000 |
| | | | | Construction Cost = | \$3,479,000 |
| | | | | Contingency (20%) = | \$695,800 |
| | | | | Sales Tax (8.7%) = | \$363,000 |
| | | | | Total Estimated Construction Cost = | \$4,538,000 |
| | | | | Permitting Fees, Engineering, Survey, etc. (15%) | \$681,000 |
| | | | | Rough Estimate of Project Total | \$5,220,000 |

Option 3: Cure In Place Pipe (CIPP)

| NO. | ITEM | UNIT | UNIT COST | PROJECT TOTAL | |
|-----|---|------|---------------|---------------|-------------|
| | | | | QUANTITY | TOTAL COST |
| 1 | Mobilization | LS | \$ 156,100.00 | 1 | \$156,100 |
| 2 | Project Temporary Traffic Control | LS | \$ 10,000.00 | 1 | \$10,000 |
| 3 | Connection to existing waterline | EA | \$ 3,500.00 | 11 | \$38,500 |
| 4 | Water Line Inspection & De-scaling | LF | \$ 25.00 | 15,595 | \$389,875 |
| 4 | Cure In Place Pipe - 6" Diameter | LF | \$ 125.00 | 16,595 | \$2,074,375 |
| 5 | Temporary Water Service | LS | \$ 100,000.00 | 1 | \$100,000 |
| 6 | PRV Stations | LS | \$ 40,000.00 | 3 | \$120,000 |
| 7 | Directional Drill - Road Bores and Slope Installation | LF | \$ 300.00 | 200 | \$60,000 |
| 8 | Water Service | EA | \$ 1,500.00 | 173 | \$259,500 |
| 9 | Sample Stations | EA | \$ 5,000.00 | 4 | \$20,000 |
| 10 | Fire Hydrants | EA | \$ 5,000.00 | 10 | \$50,000 |

| | |
|--|--------------------|
| Construction Cost = | \$3,278,000 |
| Contingency (20%) = | \$655,600 |
| Sales Tax (8.7%) = | \$342,000 |
| Total Estimated Construction Cost = | \$4,276,000 |

Permitting Fees, Engineering, Survey, etc. (15%) **\$641,000**

Rough Estimate of Project Total **\$4,920,000**

Life Cycle Cost Estimate

LIFE CYCLE COST ANALYSIS
CLIENT: Scatchet Head Water District
PROJECT: Main Replacement
DATE: October 2020

| | |
|------------------|------|
| Inflation (%/yr) | 2.5% |
|------------------|------|

| Category | Alternative | Capital Cost | Annual O&M Cost | PV of O&M Costs | Lifespan (years) | NPV |
|-------------------------|---|--------------|-----------------|-----------------|------------------|-------------|
| Distribution | #1) Main Replacement | \$2,810,000 | \$5,000 | \$155,000 | 60 | \$2,965,000 |
| | #2) Pipe Bursting | \$5,220,000 | \$5,000 | \$155,000 | 60 | \$5,375,000 |
| | #3) Slip lining | \$4,920,000 | \$5,000 | \$155,000 | 60 | \$5,075,000 |
| | #4) Do Nothing | \$0 | \$20,000 | \$618,000 | 60 | \$618,000 |
| Pumphouse and Treatment | #1) Improvements with Greensand Plus Filter Bedding | \$40,000 | \$4,800 | \$59,000 | 15 | \$99,000 |
| | #2) Improvements with New ATEC Filtration System | \$140,000 | \$4,800 | \$59,000 | 15 | \$199,000 |
| Source | #1) Well pump, piping, and meter replacement | \$80,000 | \$1,000 | \$16,000 | 20 | \$96,000 |

PV = Present Value

NPV = Net Present Value

APPENDIX E Water Use Efficiency Reports



Date Submitted: 6/27/2018

Water Use Efficiency Annual Performance Report - 2017

WS Name: SCATCHET HEAD WATER DISTRICT Water System ID# : 76470 WS County: ISLAND

Report submitted by: *Sandra Bodamer*

Meter Installation Information:

Estimate the percentage of metered connections: *100%*

If not fully metered - Current status of meter installation:

Production, Authorized Consumption, and Distribution System Leakage Information:

12-Month WUE Reporting Period: *12/01/1916* To *11/30/1917*

Incomplete or missing data for the year? *No*

If yes, explain:

Distribution System Leakage Summary:

| | |
|--|--------------------|
| Total Water Produced and Purchased (TP) – Annual Volume | 20,367,292 gallons |
| Authorized Consumption (AC) – Annual Volume | 17,896,618 gallons |
| Distribution System Leakage – Annual Volume TP – AC | 2,470,674 gallons |
| Distribution System Leakage – Percent DSL = [(TP – AC) / TP] x 100 | 12.1 % |
| 3-year annual average | 11.1 % |

Goal-Setting Information:

Date of Most Recent Public Forum: _____ Has goal been changed since last performance report? *No*

Note: Customer goal must be re-established every 6 years through a public process

WUE Goals:

Customer Goal (Demand Side):

Maintain average usage per house at 122 gpd through 2018 - actual for 2012 was 108 gpdph and 2011 was 112 gpdph.

Describe Progress in Reaching Goals:

Customer (Demand Side) Goal Progress:

Average usage per day per house was 136 gpd, this was attributable to a contractor installing a new cable throughout the entire neighborhood and breaking the line on numerous times.

Additional Information Regarding Supply and Demand Side WUE Efforts

Include any other information that describes how you and your customers use water efficiently:



Date Submitted: 6/29/2019

Water Use Efficiency Annual Performance Report - 2018

WS Name: SCATCHET HEAD WATER DISTRICT Water System ID# : 76470 WS County: ISLAND

Report submitted by: *Sandra Bodamer*

Meter Installation Information:

Estimate the percentage of metered connections: *100%*

If not fully metered - Current status of meter installation:

Production, Authorized Consumption, and Distribution System Leakage Information:

12-Month WUE Reporting Period: *01/01/2018* To *12/31/2018*

Incomplete or missing data for the year? *No*

If yes, explain:

Distribution System Leakage Summary:

| | |
|--|--------------------|
| Total Water Produced and Purchased (TP) – Annual Volume | 21,882,590 gallons |
| Authorized Consumption (AC) – Annual Volume | 18,599,325 gallons |
| Distribution System Leakage – Annual Volume TP – AC | 3,283,265 gallons |
| Distribution System Leakage – Percent DSL = [(TP – AC) / TP] x 100 | 15.0 % |
| 3-year annual average | 13.6 % |

Goal-Setting Information:

Date of Most Recent Public Forum: _____ Has goal been changed since last performance report? *No*

Note: Customer goal must be re-established every 6 years through a public process

WUE Goals:

Customer Goal (Demand Side):

Maintain average usage per house at 122 gpd through 2018 - actual for 2012 was 108 gpdph and 2011 was 112 gpdph.

Describe Progress in Reaching Goals:

Customer (Demand Side) Goal Progress:

Average usage per house per day was 146 gpd. This is above the goal of 122 gpd, due to ten leaks that were repaired in 2018 and a house fire.

Additional Information Regarding Supply and Demand Side WUE Efforts

Include any other information that describes how you and your customers use water efficiently:



Date Submitted: 6/30/2020

Water Use Efficiency Annual Performance Report - 2019

WS Name: SCATCHET HEAD WATER DISTRICT Water System ID# : 76470 WS County: ISLAND

Report submitted by: *Sandra Bodamer*

Meter Installation Information:

Estimate the percentage of metered connections: *100%*

If not fully metered - Current status of meter installation:

Production, Authorized Consumption, and Distribution System Leakage Information:

12-Month WUE Reporting Period: *12/01/2018* To *11/30/2019*

Incomplete or missing data for the year? *No*

If yes, explain:

Distribution System Leakage Summary:

| | |
|--|---------------------------|
| Total Water Produced and Purchased (TP) – Annual Volume | <i>20,757,449</i> gallons |
| Authorized Consumption (AC) – Annual Volume | <i>17,830,988</i> gallons |
| Distribution System Leakage – Annual Volume TP – AC | <i>2,926,461</i> gallons |
| Distribution System Leakage – Percent DSL = [(TP – AC) / TP] x 100 | <i>14.1 %</i> |
| 3-year annual average | <i>13.7 %</i> |

Goal-Setting Information:

Date of Most Recent Public Forum: _____ Has goal been changed since last performance report? *No*

Note: Customer goal must be re-established every 6 years through a public process

WUE Goals:

Customer Goal (Demand Side):

Maintain average usage per house at 122 gpd through 2018 - actual for 2012 was 108 gpdph and 2011 was 112 gpdph.

Describe Progress in Reaching Goals:

Customer (Demand Side) Goal Progress:

Customer demand was 139 gpd per consumer. This is slightly above goal. Have increased the rate structures to have with conservation.

Additional Information Regarding Supply and Demand Side WUE Efforts

Include any other information that describes how you and your customers use water efficiently:

In the process of securing loans to replace all main distribution lines.

APPENDIX F Water Quality Results



HYDROGEOLOGIC DATABASE Chemical Analysis

Sample Results
Color Code Legend

[Click HERE to View Information for Well 4WG](#)

Sample Exceeds } [None
Secondary MCL
Primary



Owner Name: Dept. of Natural Resources

Well Key: 4WG Site Type: Well w/in W TRS: 28N/03E-15F

PWS Name: Scatchet Head Water District

DOH PwsID: 76470 DOH Source #: 2

| Source | Date | Bicarbonate | | | Conductivity | | Hardness | | Turbidity | | | | | |
|--------|------------|-------------|--------|----|--------------|-----|----------|-----|-----------|------|-----|-------|------|-----|
| | | Alk | As | Ca | Cl | Fe | K | Mg | Mn | Na | NO3 | SO4 | TDS | |
| DOE | 12/16/1984 | | | | 14 | | | | | | | | | |
| DOE | 4/1/1985 | | | | 10 | | | | | | | | | |
| DOH | 8/12/1985 | | | | 10 | | | | | | | | | |
| DOH | 2/10/1986 | | 0.014 | | < 10 | 400 | 0.19 | 130 | | 0.18 | 41 | < 0.2 | | 1 |
| DOE | 4/14/1986 | | | | 90 | | | | | | | | | |
| DOH | 10/27/1986 | | | | 180 | | | | | | | | | |
| DOH | 4/28/1987 | | | | 10 | | | | | | | | | |
| DOH | 11/9/1987 | | | | < 10 | | | | | | | | | |
| DOH | 5/9/1988 | | | | 13 | | | | | | | | | |
| DOE | 8/29/1988 | | | | 10 | | | | | | | | | |
| DOH | 4/28/1989 | | | | 10 | 400 | | | | | | | | |
| DOH | 8/18/1989 | | | | < 10 | 390 | | | | | | | | |
| DOE | 4/15/1990 | | | | 10 | | | | | | | | | |
| DOH | 8/27/1990 | | | | 15 | 410 | | | | | | | | |
| DOH | 4/22/1991 | | | | 9 | 410 | | | | | | | | |
| DOH | 8/26/1991 | | | | 10 | 410 | | | | | | | | |
| DOH | 4/20/1992 | | | | 10 | 410 | | | | | | | | |
| DOH | 10/12/1992 | | | | 11 | 410 | | | | | | | | |
| DOH | 5/10/1993 | | | | 13 | 420 | | | | | | | | |
| DOH | 9/13/1993 | | | | 9 | 420 | | | | | | | | |
| DOH | 4/11/1994 | | | | 9 | 410 | | | | | | | | |
| DOH | 5/9/1994 | | | | | | | | | | | < 0.5 | | |
| DOH | 9/12/1994 | | | | 10 | 420 | | | | | | | | |
| DOH | 5/8/1995 | | | | 9.5 | 400 | | | | | | | | |
| DOH | 11/4/1995 | | | | 10 | | | | | | | | | |
| DOH | 11/4/1995 | | | | 10 | | | | | | | | | |
| DOH | 3/3/1997 | | 0.01 | | < 20 | 410 | 0.24 | 140 | | 0.25 | 38 | < 0.5 | < 10 | 0.3 |
| DOH | 5/4/1998 | | < 0.01 | 27 | < 20 | 400 | 0.24 | 140 | 17 | 0.26 | 39 | < 0.5 | < 10 | 0.3 |
| DOH | 9/14/1998 | | | | < 20 | | | | | | | < 0.5 | | |
| DOH | 7/19/1999 | | | | < 20 | | | | | | | < 0.5 | | |

| Source | Date | Alk | Bicarbonate | | Conductivity | | Hardness | | K | Mg | Mn | Na | NO3 | SO4 | Turbidity | |
|--------|------------|-----|-------------|----|--------------|-----|----------|-----|---|----|-------|----|-------|------|-----------|--|
| | | | As | Ca | Cl | Fe | TDS | | | | | | | | | |
| DOH | 2/14/2000 | | 0.01 | 26 | < 20 | 400 | 0.24 | 130 | | 17 | 0.26 | 38 | < 0.5 | < 10 | 0.34 | |
| DOH | 6/12/2000 | | | | < 20 | | 0.26 | | | | 0.25 | | < 0.5 | | | |
| DOH | 5/7/2001 | | | | < 20 | | | | | | | | < 0.5 | < 10 | | |
| DOH | 10/8/2001 | | | | < 20 | | 0.28 | | | | 0.25 | | 0.6 | | | |
| DOH | 2/19/2002 | | | | | | 0.038 | | | | 0.031 | | | | | |
| DOH | 3/17/2002 | | | | | | < 0.1 | | | | 0.11 | | | | | |
| DOH | 3/17/2002 | | | | | | < 0.1 | | | | 0.13 | | | | | |
| DOH | 4/1/2002 | | | | | | < 0.1 | | | | 0.063 | | | | | |
| DOH | 4/1/2002 | | | | | | 0.35 | | | | 0.24 | | < 0.5 | | | |
| DOH | 5/15/2002 | | | | | | < 0.021 | | | | 0.008 | | | | | |
| DOH | 8/12/2002 | | 0.007 | | < 20 | | | | | | | | < 0.5 | | | |
| DOH | 9/4/2002 | | | | | | 0.65 | | | | 0.021 | | | | | |
| DOH | 9/4/2002 | | | | | | < 0.021 | | | | 0.017 | | | | | |
| DOH | 9/25/2002 | | | | | | 0.025 | | | | 0.014 | | | | | |
| DOH | 9/25/2002 | | | | | | 0.1 | | | | 0.014 | | | | | |
| DOH | 10/23/2002 | | | | | | 0.242 | | | | 0.018 | | | | | |
| DOH | 10/23/2002 | | | | | | 0.03 | | | | 0.02 | | | | | |
| DOH | 11/27/2002 | | | | | | 0.19 | | | | 0.012 | | | | | |
| DOH | 11/27/2002 | | | | | | 0.029 | | | | 0.009 | | | | | |
| DOH | 12/18/2002 | | | | | | < 0.021 | | | | 0.009 | | | | | |
| DOH | 12/18/2002 | | | | | | 0.3 | | | | 0.008 | | | | | |
| DOH | 1/22/2003 | | | | | | 0.04 | | | | 0.011 | | | | | |
| DOH | 1/22/2003 | | | | | | 0.25 | | | | 0.019 | | | | | |
| DOH | 2/3/2003 | | | | | | | | | | | | < 0.5 | | | |
| DOH | 2/19/2003 | | | | | | 0.5 | | | | 0.023 | | | | | |
| DOH | 3/12/2003 | | | | | | 0.037 | | | | 0.037 | | | | | |
| DOH | 3/12/2003 | | | | | | 0.22 | | | | 0.037 | | | | | |
| DOH | 4/15/2003 | | | | | | 0.031 | | | | 0.034 | | | | | |
| DOH | 4/15/2003 | | | | | | 0.027 | | | | 0.025 | | | | | |
| DOH | 5/21/2003 | | | | | | < 0.021 | | | | 0.02 | | | | | |
| DOH | 5/21/2003 | | | | | | 0.038 | | | | 0.02 | | | | | |
| DOH | 6/16/2003 | | | | | | < 0.1 | | | | 0.036 | | | | | |
| DOH | 6/16/2003 | | | | | | < 0.1 | | | | | | | | 0.2 | |
| DOH | 7/6/2003 | | | | | | < 0.1 | | | | 0.07 | | | | | |
| DOH | 7/6/2003 | | | | | | < 0.1 | | | | 0.053 | | | | | |
| DOH | 7/15/2003 | | | | | | 0.059 | | | | 0.067 | | | | | |

| Source | Date | Bicarbonate | | | Conductivity | | Hardness | | | Turbidity | | | |
|--------|------------|-------------|----|----|--------------|---------|----------|----|-------|-----------|-----|-----|-----|
| | | Alk | As | Ca | Cl | Fe | K | Mg | Mn | Na | NO3 | SO4 | TDS |
| DOH | 7/15/2003 | | | | | 0.078 | | | 0.076 | | | | |
| DOH | 8/11/2003 | | | | | 0.16 | | | 0.036 | | | | |
| DOH | 8/11/2003 | | | | | < 0.1 | | | 0.028 | | | | |
| DOH | 8/11/2003 | | | | < 20 | | | | | < 0.5 | | | |
| DOH | 9/10/2003 | | | | | 0.052 | | | 0.032 | | | | |
| DOH | 9/10/2003 | | | | | 0.052 | | | 0.029 | | | | |
| DOH | 10/21/2003 | | | | | 0.039 | | | 0.022 | | | | |
| DOH | 10/21/2003 | | | | | 0.039 | | | 0.023 | | | | |
| DOH | 11/11/2003 | | | | | 1.1 | | | 0.029 | | | | |
| DOH | 11/11/2003 | | | | | 0.062 | | | 0.031 | | | | |
| DOH | 12/9/2003 | | | | | 0.04 | | | 0.032 | | | | |
| DOH | 12/9/2003 | | | | | 0.023 | | | 0.028 | | | | |
| DOH | 1/13/2004 | | | | | 0.058 | | | 0.034 | | | | |
| DOH | 1/13/2004 | | | | | 0.047 | | | 0.031 | | | | |
| DOH | 2/3/2004 | | | | | 0.049 | | | 0.062 | | | | |
| DOH | 2/3/2004 | | | | | 0.067 | | | 0.091 | | | | |
| DOH | 2/15/2004 | | | | | < 0.1 | | | 0.028 | | | | |
| DOH | 2/15/2004 | | | | | < 0.1 | | | 0.035 | | | | |
| DOH | 3/2/2004 | | | | | 0.041 | | | 0.021 | | | | |
| DOH | 3/2/2004 | | | | | < 0.021 | | | 0.022 | | | | |
| DOH | 4/6/2004 | | | | | 0.056 | | | 0.04 | | | | |
| DOH | 4/6/2004 | | | | | 0.046 | | | 0.024 | | | | |
| DOH | 4/20/2004 | | | | | 0.053 | | | 0.022 | | | | |
| DOH | 4/20/2004 | | | | | 0.049 | | | 0.025 | | | | |
| DOH | 5/11/2004 | | | | | 0.047 | | | 0.024 | | | | |
| DOH | 5/11/2004 | | | | | 0.047 | | | 0.062 | | | | |
| DOH | 6/1/2004 | | | | | 0.037 | | | 0.018 | | | | |
| DOH | 6/1/2004 | | | | | 0.062 | | | 0.02 | | | | |
| DOH | 7/13/2004 | | | | | 0.05 | | | 0.032 | | | | |
| DOH | 7/13/2004 | | | | | 0.056 | | | 0.023 | | | | |
| DOH | 8/4/2004 | | | | | 0.086 | | | 0.025 | | | | |
| DOH | 8/4/2004 | | | | | 0.096 | | | 0.03 | | | | |
| DOH | 9/14/2004 | | | | | 0.058 | | | 0.013 | | | | |
| DOH | 9/14/2004 | | | | | 0.22 | | | 0.25 | | | | |
| DOH | 9/14/2004 | | | | | 0.1 | | | 0.009 | | | | |
| DOH | 10/6/2004 | | | | | 0.053 | | | 0.009 | | | | |

| Source | Date | Bicarbonate | | | Conductivity | | Hardness | | | Turbidity | | | |
|--------|------------|-------------|---------|----|--------------|---------|----------|----|----|-----------|-------|-----|-------|
| | | Alk | As | Ca | Cl | Fe | K | Mg | Mn | Na | NO3 | SO4 | TDS |
| DOH | 11/2/2004 | | | | | 0.043 | | | | 0.014 | | | |
| DOH | 11/2/2004 | | | | | 0.045 | | | | 0.012 | | | |
| DOH | 12/15/2004 | | | | | < 0.021 | | | | 0.006 | | | |
| DOH | 12/15/2004 | | | | | 0.044 | | | | 0.009 | | | |
| DOH | 1/5/2005 | | | | | 0.053 | | | | 0.005 | | | |
| DOH | 1/5/2005 | | | | | 0.048 | | | | 0.008 | | | |
| DOH | 3/9/2005 | | | | | 0.041 | | | | 0.007 | | | |
| DOH | 3/9/2005 | | | | | 0.044 | | | | 0.009 | | | |
| DOH | 4/5/2005 | | | | | 0.041 | | | | 0.007 | | | |
| DOH | 4/5/2005 | | | | | 0.055 | | | | 0.007 | | | |
| DOH | 5/10/2005 | | | | | 0.069 | | | | 0.015 | | | |
| DOH | 5/10/2005 | | | | | 0.055 | | | | 0.02 | | | |
| DOH | 6/8/2005 | | | | | 0.092 | | | | < 0.005 | | | |
| DOH | 6/8/2005 | | | | | 0.042 | | | | < 0.005 | | | |
| DOH | 7/6/2005 | | | | | 0.12 | | | | 0.006 | | | |
| DOH | 7/6/2005 | | | | | 0.064 | | | | 0.005 | | | |
| DOH | 8/16/2005 | | | | | 0.023 | | | | 0.006 | | | |
| DOH | 8/16/2005 | | | | | 0.043 | | | | 0.006 | | | |
| DOH | 10/4/2005 | | | | | < 0.021 | | | | 0.017 | | | |
| DOH | 10/4/2005 | | | | | 0.046 | | | | 0.018 | | | |
| DOH | 11/2/2005 | | | | | 0.033 | | | | 0.012 | | | |
| DOH | 11/2/2005 | | | | | 0.082 | | | | 0.012 | | | |
| DOH | 12/13/2005 | | | | | < 0.021 | | | | 0.022 | | | |
| DOH | 12/13/2005 | | | | | 0.042 | | | | 0.016 | | | |
| DOH | 1/4/2006 | | | | | 0.047 | | | | 0.018 | | | |
| DOH | 1/4/2006 | | | | | 0.12 | | | | 0.047 | | | |
| DOH | 2/1/2006 | | < 0.002 | | < 20 | < 10 | 0.068 | | | 0.039 | < 0.5 | | < 0.1 |
| DOH | 2/1/2006 | | < 0.002 | | < 20 | < 10 | 0.069 | | | 0.041 | < 0.5 | | < 0.1 |
| DOH | 3/7/2006 | | | | | | 0.07 | | | 0.054 | | | |
| DOH | 3/7/2006 | | | | | | 0.11 | | | 0.054 | | | |
| DOH | 4/4/2006 | | | | | | 0.059 | | | 0.024 | | | |
| DOH | 4/4/2006 | | | | | | 0.076 | | | 0.028 | | | |
| DOH | 5/9/2006 | | | | | | 0.047 | | | 0.013 | | | |
| DOH | 5/9/2006 | | | | | | 0.092 | | | 0.017 | | | |
| DOH | 6/6/2006 | | | | | | 0.048 | | | 0.034 | | | |
| DOH | 6/6/2006 | | | | | | 0.082 | | | 0.024 | | | |

| Source | Date | Bicarbonate | | | Conductivity | | Hardness | | | Turbidity | | | |
|----------------------------------|------------|-------------|-------|------------|--------------|------------------|----------|-------------|-------|-----------|-----|-----|-----|
| | | Alk | As | Ca | Cl | Fe | K | Mg | Mn | Na | NO3 | SO4 | TDS |
| DOH | 7/4/2006 | | | | | 0.074 | | | 0.027 | | | | |
| DOH | 7/4/2006 | | | | | 0.078 | | | 0.032 | | | | |
| DOH | 8/2/2006 | | | | | 0.069 | | | 0.038 | | | | |
| DOH | 8/2/2006 | | | | | 0.054 | | | 0.039 | | | | |
| DOH | 9/12/2006 | | | | | 0.12 | | | 0.068 | | | | |
| DOH | 9/12/2006 | | | | | 0.12 | | | 0.092 | | | | |
| DOH | 10/4/2006 | | | | | 0.064 | | | 0.034 | | | | |
| DOH | 10/4/2006 | | | | | 0.16 | | | 0.034 | | | | |
| DOH | 12/12/2006 | | | | | 0.064 | | | 0.031 | | | | |
| DOH | 12/12/2006 | | | | | 0.096 | | | 0.026 | | | | |
| DOH | 1/10/2007 | | | | | 0.055 | | | 0.054 | | | | |
| DOH | 1/10/2007 | | | | | 0.051 | | | 0.064 | | | | |
| DOH | 9/13/2010 | | 0.009 | | | 0.35 | | | 0.22 | | | | |
| DOH | 4/27/2020 | | | | < 20 | 363 | | | | | | | |
| DOH | 8/31/2020 | | | | < 20 | 363 | | | | | | | |
| Select Summary Statistics | | Avg As: | 0.007 | Avg Cl: | 16.3 | Avg Hardness: | 135 | Avg NO3: | 0.26 | | | | |
| | | Median As: | 0.008 | Median Cl: | 10.0 | Median Hardness: | 135 | Median NO3: | 0.25 | | | | |
| | | Max As: | 0.014 | Max Cl: | 180.0 | Max Hardness: | 140 | Max NO3: | 0.6 | | | | |

Bacteria Samples (distribution): [381 sample\(s\)](#)

Disclaimer: Data presented has been collected from a variety of sources. Island County makes no guarantee as to the validity or accuracy of this data. Please report any errors to the Island County Hydrogeologist.

Generated by the Island County Hydrogeologic Database

153 records printed on 10/6/2020

Note: Items with [blue frames and blue text](#) are clickable hyperlinks to additional information / resources.

Parameter labels with a [red fill color](#) are exhibiting an increasing trend, and those with a [green fill color](#) are exhibiting a decreasing trend.



HYDROGEOLOGIC DATABASE Chemical Analysis

Sample Results Color Code Legend

Sample Exceeds None Secondary Primary MCL



[Click HERE to View Information for Well 4WH](#)

Owner Name: **Scatchet Head Water District**

Well Key: **4WH** Site Type: **Well w/in W** TRS: **28N/03E-15F**

PWS Name: **Scatchet Head Water District**

DOH PwsID: 76470 DOH Source #: **3**

| Source | Date | Bicarbonate | | | Conductivity | | Hardness | | | Turbidity | | | | | |
|--------|-----------|-------------|-------|----|--------------|-----|----------|----|----|-----------|-------|-----|-------|--|-----|
| | | Alk | As | Ca | Cl | Fe | K | Mg | Mn | Na | NO3 | SO4 | TDS | | |
| DOH | 11/4/1995 | | 0.016 | | 11 | 374 | < 0.03 | 80 | | | 0.127 | 53 | < 0.2 | | 0.2 |
| DOH | 1/21/1997 | | | | 11 | 320 | 2.2 | | | | 0.13 | | | | 190 |
| DOH | 7/19/1999 | | | | < 20 | | | | | | | | < 0.5 | | |
| DOH | 8/12/2002 | | 0.004 | | < 20 | | | | | | | | < 0.5 | | |
| DOH | 7/6/2003 | | | | | | < 0.1 | | | | 0.07 | | | | |
| DOH | 7/6/2003 | | | | | | < 0.1 | | | | 0.053 | | | | |
| DOH | 7/15/2003 | | | | | | 0.059 | | | | 0.067 | | | | |
| DOH | 7/15/2003 | | | | | | 0.078 | | | | 0.076 | | | | |
| DOH | 8/11/2003 | | | | < 20 | | | | | | | | < 0.5 | | |
| DOH | 10/4/2005 | | | | | | < 0.021 | | | | 0.017 | | | | |
| DOH | 11/2/2005 | | | | | | 0.082 | | | | 0.012 | | | | |
| DOH | 11/2/2005 | | | | | | 0.033 | | | | 0.012 | | | | |
| DOH | 9/13/2010 | | 0.02 | | | | 0.36 | | | | 0.2 | | | | |
| DOH | 4/30/2020 | | | | < 20 | 384 | | | | | | | | | |
| DOH | 8/31/2020 | | | | < 20 | 361 | | | | | | | | | |

| | | | | | | | | |
|----------------------------------|------------|-------|------------|------|------------------|----|-------------|------|
| Select Summary Statistics | Avg As: | 0.013 | Avg Cl: | 10.3 | Avg Hardness: | 80 | Avg NO3: | 0.21 |
| | Median As: | 0.016 | Median Cl: | 10.0 | Median Hardness: | 80 | Median NO3: | 0.25 |
| | Max As: | 0.02 | Max Cl: | 11.0 | Max Hardness: | 80 | Max NO3: | 0.25 |

Bacteria Samples (distribution): [381 sample\(s\)](#)

Disclaimer: Data presented has been collected from a variety of sources. Island County makes no guarantee as to the validity or accuracy of this data. Please report any errors to the Island County Hydrogeologist.

Generated by the Island County Hydrogeologic Database

15 records printed on 10/6/2020

Note: Items with blue frames and blue text are clickable hyperlinks to additional information / resources.

Parameter labels with a red fill color are exhibiting an increasing trend, and those with a green fill color are exhibiting a decreasing trend.

APPENDIX G Hydraulic Model

Hydraulic Model - Scatchet Head Water District



| Junction ID | Elevation (ft) | Scenario 1: Static Water Pressure | | Scenario 2: Peak Hour Demand | | Scenario 3: Fire-flow and MDD | |
|-------------|----------------|-----------------------------------|----------------|------------------------------|----------------|-------------------------------|----------------|
| | | Demand (gpm) | Pressure (psi) | Demand (gpm) | Pressure (psi) | Demand (gpm) | Pressure (psi) |
| J-83 | 360 | 0 | 31 | 0 | 31 | 0 | 31 |
| J-84 | 360 | 0 | 31 | 0 | 31 | 0 | 31 |
| J-85 | 360 | 0 | 31 | 0 | 31 | 0 | 31 |
| J-86 | 360 | 0 | 31 | 0 | 31 | 0 | 31 |
| J-69 | 190 | 0 | 40 | 0 | 40 | 0 | 40 |
| J-64 | 230 | 0 | 42 | 9 | 41 | 4 | 41 |
| J-77 | 185 | 0 | 42 | 0 | 42 | 0 | 42 |
| J-78 | 170 | 0 | 49 | 6 | 49 | 3 | 49 |
| J-1 | 368 | 0 | 52 | 7 | 41 | 0 | 39 |
| J-2 | 365 | 0 | 53 | 8 | 42 | 4 | 39 |
| J-35 | 365 | 0 | 53 | 0 | 42 | 0 | 39 |
| J-36 | 365 | 0 | 53 | 5 | 42 | 2 | 39 |
| J-72 | 160 | 0 | 53 | 0 | 53 | 0 | 53 |
| J-7 | 360 | 0 | 55 | 8 | 44 | 4 | 41 |
| J-8 | 360 | 0 | 55 | 6 | 44 | 3 | 41 |
| J-33 | 360 | 0 | 55 | 4 | 44 | 2 | 41 |
| J-34 | 360 | 0 | 55 | 0 | 44 | 0 | 41 |
| J-87 | 360 | 0 | 55 | 0 | 45 | 0 | 45 |
| J-88 | 360 | 0 | 55 | 0 | 45 | 0 | 44 |
| J-89 | 360 | 0 | 55 | 0 | 45 | 0 | 44 |
| J-90 | 360 | 0 | 55 | 0 | 45 | 0 | 44 |
| J-75 | 20 | 0 | 55 | 7 | 55 | 3 | 55 |
| J-76 | 20 | 0 | 55 | 8 | 55 | 4 | 55 |
| J-80 | 20 | 0 | 55 | 2 | 55 | 1 | 55 |
| J-81 | 20 | 0 | 55 | 5 | 55 | 2 | 55 |
| J-82 | 20 | 0 | 55 | 21 | 55 | 10 | 55 |
| J-23 | 355 | 0 | 57 | 0 | 46 | 0 | 42 |
| J-24 | 355 | 0 | 57 | 0 | 46 | 0 | 42 |
| J-25 | 355 | 0 | 57 | 0 | 46 | 0 | 43 |
| J-26 | 355 | 0 | 57 | 6 | 46 | 3 | 43 |
| J-39 | 355 | 0 | 57 | 8 | 46 | 4 | 42 |
| J-40 | 355 | 0 | 57 | 0 | 46 | 0 | 42 |
| J-13 | 352 | 0 | 58 | 7 | 47 | 3 | 44 |
| J-31 | 352 | 0 | 58 | 3 | 47 | 1 | 44 |
| J-9 | 350 | 0 | 59 | 0 | 48 | 0 | 45 |
| J-27 | 350 | 0 | 59 | 3 | 48 | 1 | 45 |
| J-30 | 350 | 0 | 59 | 0 | 48 | 0 | 45 |
| J-38 | 350 | 0 | 59 | 4 | 48 | 2 | 45 |
| J-41 | 350 | 0 | 59 | 4 | 48 | 2 | 45 |
| J-42 | 350 | 0 | 59 | 2 | 48 | 1 | 45 |
| J-43 | 350 | 0 | 59 | 1 | 48 | 1 | 45 |
| J-45 | 350 | 0 | 59 | 7 | 48 | 3 | 45 |
| J-46 | 350 | 0 | 59 | 7 | 48 | 3 | 45 |

| Junction ID | Elevation (ft) | Scenario 1: Static Water Pressure | | Scenario 2: Peak Hour Demand | | Scenario 3: Fire-flow and MDD | |
|-------------|----------------|-----------------------------------|----------------|------------------------------|----------------|-------------------------------|----------------|
| | | Demand (gpm) | Pressure (psi) | Demand (gpm) | Pressure (psi) | Demand (gpm) | Pressure (psi) |
| J-70 | 145 | 0 | 59 | 11 | 59 | 5 | 59 |
| J-12 | 347 | 0 | 61 | 0 | 50 | 0 | 46 |
| J-3 | 345 | 0 | 61 | 0 | 51 | 0 | 48 |
| J-10 | 345 | 0 | 61 | 7 | 51 | 3 | 48 |
| J-11 | 345 | 0 | 61 | 0 | 50 | 0 | 47 |
| J-71 | 140 | 0 | 62 | 6 | 62 | 3 | 62 |
| J-5 | 340 | 0 | 64 | 11 | 53 | 5 | 50 |
| J-6 | 340 | 0 | 64 | 0 | 53 | 0 | 50 |
| J-14 | 340 | 0 | 64 | 5 | 53 | 2 | 48 |
| J-21 | 340 | 0 | 64 | 3 | 53 | 1 | 48 |
| J-22 | 340 | 0 | 64 | 0 | 53 | 0 | 48 |
| J-29 | 340 | 0 | 64 | 3 | 52 | 1 | 49 |
| J-32 | 340 | 0 | 64 | 4 | 53 | 2 | 50 |
| J-44 | 340 | 0 | 64 | 0 | 52 | 0 | 49 |
| J-54 | 340 | 0 | 64 | 0 | 52 | 0 | 49 |
| J-55 | 340 | 0 | 64 | 3 | 52 | 1 | 49 |
| J-73 | 135 | 0 | 64 | 6 | 64 | 3 | 64 |
| J-63 | 175 | 0 | 65 | 0 | 65 | 0 | 65 |
| J-28 | 335 | 0 | 66 | 1 | 55 | 1 | 51 |
| J-37 | 335 | 0 | 66 | 6 | 55 | 3 | 49 |
| J-53 | 335 | 0 | 66 | 0 | 54 | 0 | 51 |
| J-58 | 335 | 0 | 66 | 1 | 54 | 1 | 51 |
| J-59 | 335 | 0 | 66 | 1 | 54 | 1 | 51 |
| J-56 | 332 | 0 | 67 | 3 | 56 | 1 | 52 |
| J-15 | 330 | 0 | 68 | 0 | 57 | 0 | 52 |
| J-16 | 330 | 0 | 68 | 0 | 57 | 0 | 51 |
| J-17 | 330 | 0 | 68 | 0 | 57 | 500 | 50 |
| J-18 | 330 | 0 | 68 | 5 | 57 | 2 | 50 |
| J-20 | 330 | 0 | 68 | 3 | 57 | 1 | 52 |
| J-52 | 330 | 0 | 68 | 4 | 56 | 2 | 53 |
| J-4 | 325 | 0 | 70 | 4 | 59 | 2 | 57 |
| J-49 | 325 | 0 | 70 | 2 | 59 | 1 | 55 |
| J-50 | 325 | 0 | 70 | 0 | 59 | 0 | 55 |
| J-51 | 325 | 0 | 70 | 6 | 59 | 3 | 55 |
| J-57 | 325 | 0 | 70 | 3 | 59 | 1 | 55 |
| J-19 | 320 | 0 | 72 | 4 | 61 | 2 | 55 |
| J-65 | 150 | 0 | 76 | 15 | 74 | 7 | 76 |
| J-60 | 300 | 0 | 81 | 13 | 69 | 6 | 66 |
| J-66 | 290 | 0 | 85 | 9 | 74 | 4 | 71 |
| J-74 | 85 | 0 | 85 | 9 | 85 | 4 | 85 |
| J-67 | 275 | 0 | 92 | 0 | 80 | 0 | 77 |
| J-61 | 250 | 0 | 103 | 1 | 91 | 1 | 88 |
| J-47 | 225 | 0 | 113 | 0 | 102 | 0 | 99 |

| Junction ID | Elevation (ft) | Scenario 1: Static Water Pressure | | Scenario 2: Peak Hour Demand | | Scenario 3: Fire-flow and MDD | |
|-------------|----------------|-----------------------------------|----------------|------------------------------|----------------|-------------------------------|----------------|
| | | Demand (gpm) | Pressure (psi) | Demand (gpm) | Pressure (psi) | Demand (gpm) | Pressure (psi) |
| J-92 | 223 | 0 | 114 | 3 | 103 | 1 | 100 |
| J-68 | 220 | 0 | 116 | 0 | 104 | 0 | 101 |
| J-79 | 215 | 0 | 118 | 0 | 106 | 0 | 103 |
| J-62 | 190 | 0 | 129 | 0 | 117 | 0 | 114 |
| J-91 | 190 | 0 | 129 | 0 | 117 | 0 | 114 |

| Pipe ID | Length (ft) | Diameter (inch) | Material | Start Node | Stop Node | Scenario 1: Static Water Pressure | | Scenario 2: Peak Hour Demand | | Scenario 3: Fire-flow and MDD | |
|---------|-------------|-----------------|--------------|------------|-----------|-----------------------------------|-----------------|------------------------------|-----------------|-------------------------------|-----------------|
| | | | | | | Flow (gpm) | Velocity (ft/s) | Flow (gpm) | Velocity (ft/s) | Flow (gpm) | Velocity (ft/s) |
| P-1 | 189 | 6 | PVC | J-1 | J-2 | 0 | 0 | 194 | 2.21 | 426 | 4.83 |
| P-2 | 130 | 6 | PVC | J-2 | J-3 | 0 | 0 | 71 | 0.8 | 145 | 1.64 |
| P-3 | 657 | 6 | PVC | J-32 | J-4 | 0 | 0 | -11 | 0.13 | -18 | 0.2 |
| P-4 | 775 | 6 | PVC | J-1 | J-5 | 0 | 0 | 96 | 1.09 | 211 | 2.4 |
| P-5 | 19 | 6 | PVC | J-5 | J-6 | 0 | 0 | 15 | 0.17 | 19 | 0.22 |
| P-6 | 579 | 6 | PVC | J-6 | J-4 | 0 | 0 | 15 | 0.17 | 19 | 0.22 |
| P-7 | 242 | 6 | PVC | J-2 | J-7 | 0 | 0 | 116 | 1.32 | 277 | 3.15 |
| P-8 | 446 | 6 | PVC | J-7 | J-8 | 0 | 0 | 19 | 0.21 | 80 | 0.91 |
| P-9 | 270 | 6 | PVC | J-8 | J-9 | 0 | 0 | 12 | 0.14 | 77 | 0.87 |
| P-11 | 249 | 6 | PVC | J-9 | J-10 | 0 | 0 | -64 | 0.73 | -184 | 2.08 |
| P-12 | 300 | 6 | PVC | J-10 | J-5 | 0 | 0 | -71 | 0.81 | -187 | 2.12 |
| P-13 | 304 | 6 | PVC | J-9 | J-11 | 0 | 0 | 76 | 0.87 | 261 | 2.96 |
| P-14 | 24 | 6 | Ductile Iron | J-11 | J-12 | 0 | 0 | 32 | 0.37 | -44 | 0.5 |
| P-15 | 293 | 6 | Ductile Iron | J-12 | J-13 | 0 | 0 | 32 | 0.37 | -44 | 0.5 |
| P-16 | 359 | 6 | PVC | J-11 | J-14 | 0 | 0 | 44 | 0.5 | 304 | 3.45 |
| P-17 | 284 | 6 | PVC | J-14 | J-15 | 0 | 0 | 14 | 0.16 | 284 | 3.23 |
| P-18 | 357 | 6 | PVC | J-15 | J-16 | 0 | 0 | 14 | 0.16 | 284 | 3.23 |
| P-19 | 134 | 6 | PVC | J-16 | J-17 | 0 | 0 | 8 | 0.09 | 282 | 3.2 |
| P-20 | 29 | 6 | PVC | J-17 | J-18 | 0 | 0 | 8 | 0.09 | -218 | 2.48 |
| P-21 | 484 | 6 | PVC | J-18 | J-19 | 0 | 0 | 3 | 0.04 | -221 | 2.5 |
| P-22 | 386 | 6 | PVC | J-19 | J-20 | 0 | 0 | -1 | 0.01 | -223 | 2.53 |
| P-23 | 318 | 6 | PVC | J-20 | J-21 | 0 | 0 | -4 | 0.04 | -224 | 2.54 |
| P-24 | 228 | 6 | PVC | J-21 | J-14 | 0 | 0 | -25 | 0.29 | -18 | 0.2 |
| P-25 | 27 | 6 | PVC | J-21 | J-22 | 0 | 0 | 19 | 0.21 | -207 | 2.35 |
| P-26 | 622 | 6 | PVC | J-22 | J-23 | 0 | 0 | 19 | 0.21 | -207 | 2.35 |
| P-27 | 20 | 6 | PVC | J-23 | J-24 | 0 | 0 | -50 | 0.57 | -125 | 1.42 |
| P-28 | 253 | 6 | PVC | J-24 | J-13 | 0 | 0 | -50 | 0.57 | -125 | 1.42 |
| P-29 | 423 | 6 | PVC | J-13 | J-25 | 0 | 0 | -25 | 0.28 | -173 | 1.96 |
| P-30 | 17 | 6 | PVC | J-25 | J-26 | 0 | 0 | -25 | 0.28 | -173 | 1.96 |
| P-31 | 281 | 6 | PVC | J-26 | J-7 | 0 | 0 | -90 | 1.02 | -194 | 2.2 |
| P-32 | 239 | 6 | PVC | J-26 | J-27 | 0 | 0 | 59 | 0.67 | 19 | 0.21 |

| Pipe ID | Length (ft) | Diameter (inch) | Material | Start Node | Stop Node | Scenario 1: Static Water Pressure | | Scenario 2: Peak Hour Demand | | Scenario 3: Fire-flow and MDD | |
|---------|-------------|-----------------|--------------|------------|-----------|-----------------------------------|-----------------|------------------------------|-----------------|-------------------------------|-----------------|
| | | | | | | Flow (gpm) | Velocity (ft/s) | Flow (gpm) | Velocity (ft/s) | Flow (gpm) | Velocity (ft/s) |
| P-33 | 300 | 6 | PVC | J-27 | J-28 | 0 | 0 | 126 | 1.43 | 174 | 1.98 |
| P-34 | 75 | 6 | PVC | J-28 | J-29 | 0 | 0 | 26 | 0.29 | 121 | 1.37 |
| P-35 | 165 | 6 | PVC | J-29 | J-30 | 0 | 0 | -66 | 0.75 | 83 | 0.95 |
| P-36 | 432 | 6 | PVC | J-30 | J-31 | 0 | 0 | -66 | 0.75 | 83 | 0.95 |
| P-37 | 349 | 6 | PVC | J-31 | J-23 | 0 | 0 | -69 | 0.78 | 82 | 0.93 |
| P-38 | 281 | 6 | PVC | J-32 | J-33 | 0 | 0 | 78 | 0.89 | 161 | 1.82 |
| P-39 | 16 | 6 | PVC | J-33 | J-34 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-40 | 67 | 6 | PVC | J-3 | J-32 | 0 | 0 | 71 | 0.8 | 145 | 1.64 |
| P-41 | 229 | 6 | PVC | J-27 | J-35 | 0 | 0 | -70 | 0.79 | -157 | 1.78 |
| P-42 | 412 | 6 | PVC | J-35 | J-33 | 0 | 0 | -75 | 0.85 | -159 | 1.8 |
| P-43 | 242 | 2 | PVC | J-35 | J-36 | 0 | 0 | 5 | 0.5 | 2 | 0.24 |
| P-44 | 225 | 2 | PVC | J-16 | J-37 | 0 | 0 | 6 | 0.57 | 3 | 0.27 |
| P-45 | 328 | 6 | PVC | J-29 | J-38 | 0 | 0 | 89 | 1.01 | 36 | 0.41 |
| P-46 | 168 | 8 | PVC | J-38 | J-39 | 0 | 0 | 86 | 0.55 | 35 | 0.22 |
| P-47 | 32 | 8 | PVC | J-39 | J-40 | 0 | 0 | 42 | 0.27 | 17 | 0.11 |
| P-48 | 170 | 8 | PVC | J-40 | J-41 | 0 | 0 | 42 | 0.27 | 17 | 0.11 |
| P-49 | 450 | 6 | PVC | J-41 | J-42 | 0 | 0 | 37 | 0.42 | 15 | 0.17 |
| P-50 | 126 | 6 | PVC | J-42 | J-43 | 0 | 0 | -35 | 0.4 | -14 | 0.16 |
| P-51 | 416 | 6 | PVC | J-43 | J-39 | 0 | 0 | -36 | 0.41 | -14 | 0.16 |
| P-52 | 185 | 6 | PVC | J-42 | J-44 | 0 | 0 | 70 | 0.8 | 27 | 0.31 |
| P-53 | 322 | 6 | PVC | J-44 | J-45 | 0 | 0 | 7 | 0.08 | 3 | 0.04 |
| P-54 | 302 | 6 | PVC | J-44 | J-46 | 0 | 0 | 63 | 0.72 | 24 | 0.27 |
| P-55 | 445 | 6 | PVC | J-46 | J-47 | 0 | 0 | 56 | 0.64 | 21 | 0.24 |
| P-57 | 432 | 6 | PVC | J-49 | J-50 | 0 | 0 | 43 | 0.49 | 20 | 0.23 |
| P-58 | 28 | 6 | Ductile Iron | J-50 | J-51 | 0 | 0 | 43 | 0.49 | 20 | 0.23 |
| P-59 | 523 | 6 | PVC | J-51 | J-52 | 0 | 0 | 26 | 0.29 | 12 | 0.14 |
| P-60 | 183 | 4 | PVC | J-52 | J-53 | 0 | 0 | 0 | 0 | 0 | 0.01 |
| P-61 | 196 | 4 | PVC | J-53 | J-54 | 0 | 0 | -2 | 0.04 | -1 | 0.02 |
| P-62 | 14 | 4 | PVC | J-54 | J-55 | 0 | 0 | -3 | 0.08 | -2 | 0.04 |
| P-63 | 260 | 4 | PVC | J-55 | J-56 | 0 | 0 | -6 | 0.15 | -3 | 0.07 |
| P-64 | 252 | 4 | PVC | J-56 | J-51 | 0 | 0 | -11 | 0.29 | -5 | 0.14 |

| Pipe ID | Length (ft) | Diameter (inch) | Material | Start Node | Stop Node | Scenario 1: Static Water Pressure | | Scenario 2: Peak Hour Demand | | Scenario 3: Fire-flow and MDD | |
|---------|-------------|-----------------|--------------|------------|-----------|-----------------------------------|-----------------|------------------------------|-----------------|-------------------------------|-----------------|
| | | | | | | Flow (gpm) | Velocity (ft/s) | Flow (gpm) | Velocity (ft/s) | Flow (gpm) | Velocity (ft/s) |
| P-65 | 151 | 2 | PVC | J-56 | J-57 | 0 | 0 | 3 | 0.29 | 1 | 0.13 |
| P-66 | 188 | 2 | PVC | J-54 | J-58 | 0 | 0 | 1 | 0.14 | 1 | 0.07 |
| P-67 | 124 | 4 | PVC | J-53 | J-59 | 0 | 0 | 1 | 0.04 | 1 | 0.02 |
| P-68 | 508 | 6 | PVC | J-47 | J-49 | 0 | 0 | 46 | 0.52 | 21 | 0.24 |
| P-69 | 673 | 7 | PVC | J-52 | J-60 | 0 | 0 | 22 | 0.18 | 10 | 0.09 |
| P-70 | 611 | 7 | PVC | J-60 | J-61 | 0 | 0 | 9 | 0.08 | 4 | 0.04 |
| P-71 | 1,092 | 7 | PVC | J-61 | J-62 | 0 | 0 | -16 | 0.14 | -8 | 0.06 |
| P-72 | 610 | 6 | PVC | PRV-4 | J-63 | 0 | 0 | 24 | 0.27 | 11 | 0.13 |
| P-73 | 474 | 2 | PVC | J-63 | J-64 | 0 | 0 | 9 | 0.93 | 4 | 0.44 |
| P-74 | 814 | 2 | PVC | J-63 | J-65 | 0 | 0 | 15 | 1.5 | 7 | 0.71 |
| P-75 | 641 | 7 | PVC | J-28 | J-66 | 0 | 0 | 99 | 0.84 | 52 | 0.44 |
| P-76 | 723 | 7 | PVC | J-66 | J-67 | 0 | 0 | 90 | 0.76 | 48 | 0.41 |
| P-77 | 442 | 7 | PVC | J-67 | J-68 | 0 | 0 | 90 | 0.76 | 48 | 0.41 |
| P-78 | 685 | 6 | PVC | J-69 | J-70 | 0 | 0 | 25 | 0.29 | 12 | 0.13 |
| P-79 | 246 | 6 | PVC | J-70 | J-71 | 0 | 0 | 5 | 0.06 | 2 | 0.03 |
| P-80 | 395 | 6 | PVC | J-71 | J-72 | 0 | 0 | -7 | 0.08 | -3 | 0.04 |
| P-81 | 184 | 2 | PVC | J-71 | J-73 | 0 | 0 | 6 | 0.64 | 3 | 0.3 |
| P-82 | 381 | 6 | PVC | J-70 | J-74 | 0 | 0 | 9 | 0.1 | 4 | 0.05 |
| P-83 | 10 | 6 | Ductile Iron | J-74 | PRV-1 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-84 | 183 | 7 | PVC | PRV-1 | J-75 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-85 | 682 | 6 | PVC | J-75 | J-76 | 0 | 0 | -7 | 0.08 | -3 | 0.04 |
| P-86 | 764 | 4 | PVC | J-77 | J-78 | 0 | 0 | 6 | 0.16 | 3 | 0.08 |
| P-87 | 27 | 7 | PVC | J-68 | J-79 | 0 | 0 | 98 | 0.83 | 46 | 0.39 |
| P-88 | 526 | 7 | PVC | J-79 | J-91 | 0 | 0 | 98 | 0.83 | 46 | 0.39 |
| P-89 | 10 | 7 | PVC | PRV-2 | J-69 | 0 | 0 | 82 | 0.69 | 39 | 0.33 |
| P-90 | 16 | 7 | PVC | J-69 | J-77 | 0 | 0 | 57 | 0.48 | 27 | 0.23 |
| P-91 | 355 | 7 | PVC | J-77 | J-72 | 0 | 0 | 50 | 0.43 | 24 | 0.2 |
| P-92 | 784 | 7 | PVC | J-72 | PRV-3 | 0 | 0 | 43 | 0.37 | 20 | 0.17 |
| P-93 | 13 | 6 | Ductile Iron | PRV-3 | J-76 | 0 | 0 | 43 | 0.49 | 20 | 0.23 |
| P-94 | 420 | 6 | PVC | J-76 | J-80 | 0 | 0 | 28 | 0.32 | 13 | 0.15 |
| P-95 | 846 | 6 | PVC | J-80 | J-81 | 0 | 0 | 26 | 0.29 | 12 | 0.14 |

| Pipe ID | Length (ft) | Diameter (inch) | Material | Start Node | Stop Node | Scenario 1: Static Water Pressure | | Scenario 2: Peak Hour Demand | | Scenario 3: Fire-flow and MDD | |
|---------|-------------|-----------------|--------------|------------|-----------|-----------------------------------|-----------------|------------------------------|-----------------|-------------------------------|-----------------|
| | | | | | | Flow (gpm) | Velocity (ft/s) | Flow (gpm) | Velocity (ft/s) | Flow (gpm) | Velocity (ft/s) |
| P-96 | 1386 | 6 | PVC | J-81 | J-82 | 0 | 0 | 21 | 0.24 | 10 | 0.11 |
| P-97 | 30 | 8 | Ductile Iron | T-1 | J-83 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-98 | 25 | 8 | Ductile Iron | J-83 | J-84 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-99 | 25 | 8 | Ductile Iron | J-84 | J-85 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-100 | 25 | 8 | Ductile Iron | J-85 | J-86 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-101 | 15 | 4 | Ductile Iron | J-86 | PMP-4 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-102 | 15 | 2 | PVC | PMP-4 | J-87 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-103 | 25 | 6 | Ductile Iron | J-87 | J-88 | 0 | 0 | 298 | 3.38 | 637 | 7.23 |
| P-104 | 25 | 6 | Ductile Iron | J-88 | J-89 | 0 | 0 | 298 | 3.38 | 637 | 7.23 |
| P-105 | 25 | 6 | Ductile Iron | J-89 | J-90 | 0 | 0 | 298 | 3.38 | 637 | 7.23 |
| P-106 | 77 | 6 | Ductile Iron | J-90 | J-1 | 0 | 0 | 297 | 3.38 | 637 | 7.23 |
| P-107 | 15 | 6 | Ductile Iron | J-83 | PMP-1 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-108 | 15 | 2 | PVC | PMP-1 | J-90 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-109 | 15 | 6 | Ductile Iron | J-84 | PMP-2 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-110 | 15 | 2 | PVC | PMP-2 | J-89 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-111 | 15 | 4 | Ductile Iron | J-85 | PMP-3 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-112 | 15 | 2 | PVC | PMP-3 | J-88 | 0 | 0 | 0 | 0 | 0 | 0 |
| P-115 | 25 | 6 | Ductile Iron | T-3 | J-87 | 0 | 0 | 298 | 3.38 | 637 | 7.23 |
| P-116 | 38 | 6 | Ductile Iron | J-91 | J-62 | 0 | 0 | 16 | 0.18 | 8 | 0.09 |
| P-117 | 12 | 6 | Ductile Iron | J-91 | PRV-2 | 0 | 0 | 82 | 0.93 | 39 | 0.44 |
| P-118 | 55 | 6 | PVC | J-61 | PRV-4 | 0 | 0 | 24 | 0.27 | 11 | 0.13 |
| P-119 | 174 | 6 | PVC | J-47 | J-92 | 0 | 0 | 11 | 0.12 | -1 | 0.01 |
| P-120 | 289 | 6 | PVC | J-92 | J-68 | 0 | 0 | 8 | 0.09 | -2 | 0.02 |